

# Added mass effect in forward and inverse fluid-structure interaction algorithms

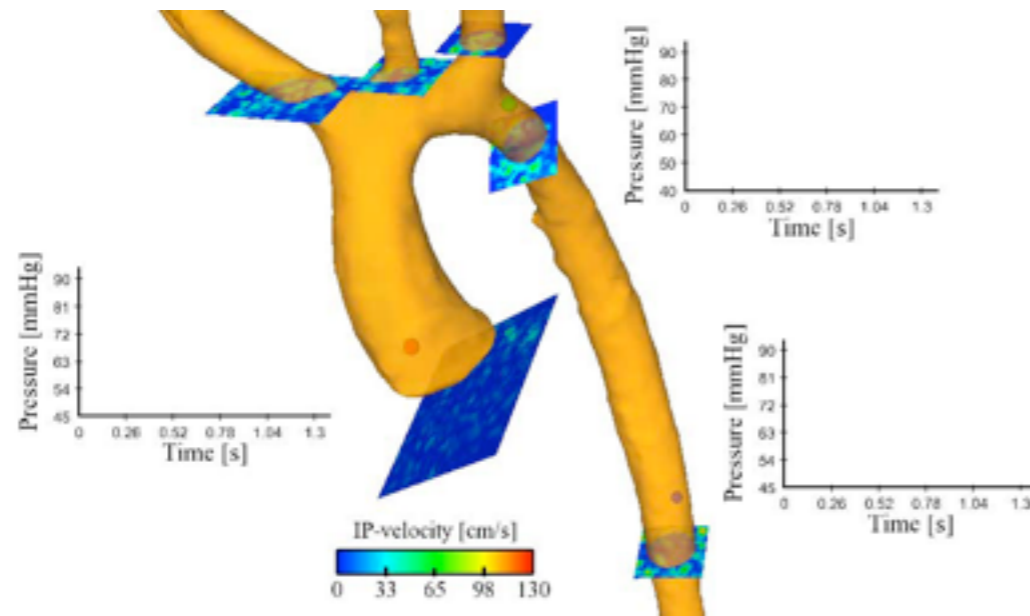
Bordeaux, January 11-14th, 2016

**Jean-Frédéric Gerbeau**

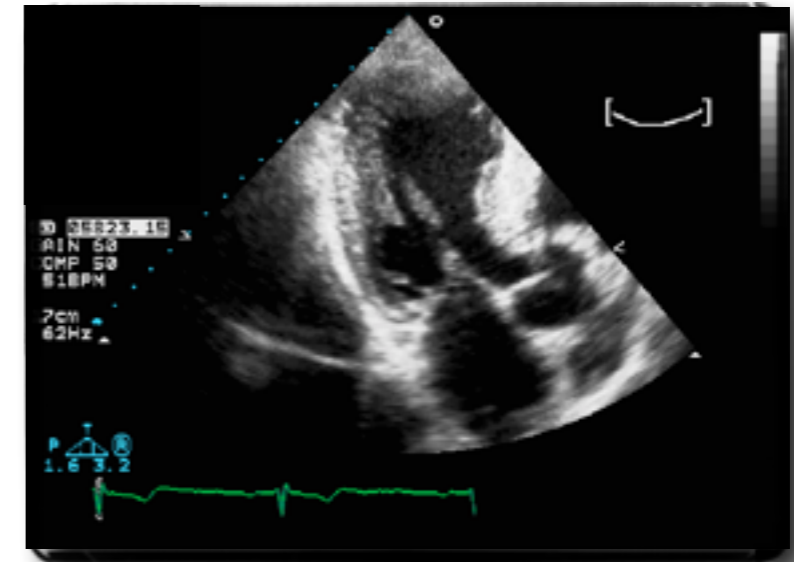
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France**



# Fluid-structure interaction in blood flows



KCL (euHeart)



Hôpital Laval

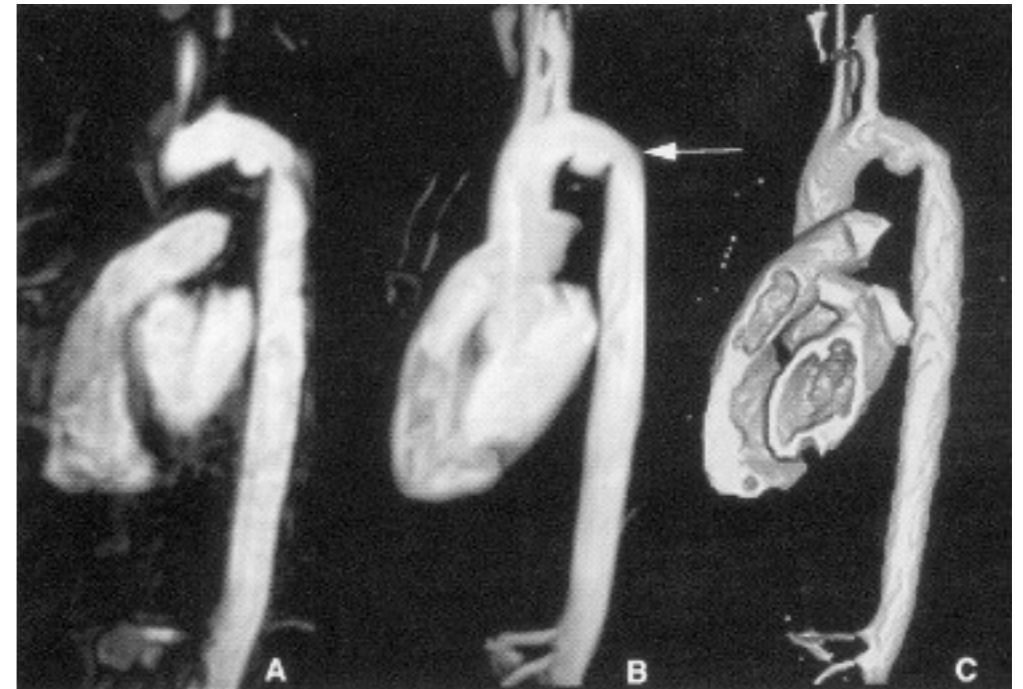
$$\rho^f \left( \frac{\partial \mathbf{u}}{\partial t} \Big|_{\hat{\mathbf{x}}} + (\mathbf{u} - \mathbf{w}) \cdot \nabla \mathbf{u} \right) - 2\mu \operatorname{div} \epsilon(\mathbf{u}) + \nabla p = \mathbf{0}, \quad \text{in } \Omega^f(t)$$

$$\operatorname{div} \mathbf{u} = 0, \quad \text{in } \Omega^f(t)$$

$$\rho^s \frac{\partial^2 \mathbf{d}}{\partial t^2} - \operatorname{div} (\mathbf{F}(\mathbf{d}) \mathbf{S}(\mathbf{d})) = \mathbf{0}, \quad \text{in } \hat{\Omega}^s$$

# Possible application: avoid clinical exams ?

- **Example:** aortic coarctation
- After surgical repair, patients must be followed on a regular basis
- Exercise test is often necessary to assess the patient condition
- **Question:** With computer simulations, can we extrapolate the rest test to avoid the stress test ?
- Maybe... **if we are able to “personalize” an FSI model of the aorta**



Source: O. Peruta

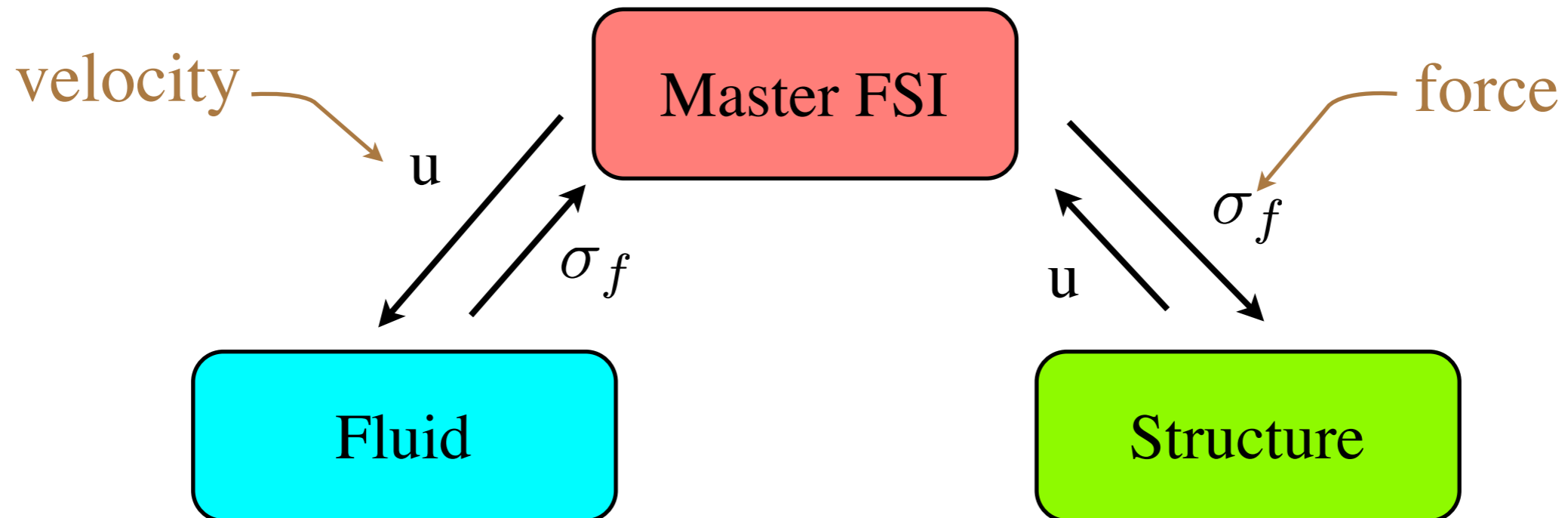
In collaboration with R. Hose (Sheffield), I. Valverde, P. Beerbaum (KCL)

# Outline

- Forward problem in Fluid-Structure Interaction
- Inverse problem in Fluid-Structure Interaction

# Fluid-Structure coupling

- **Partitioned approach:**



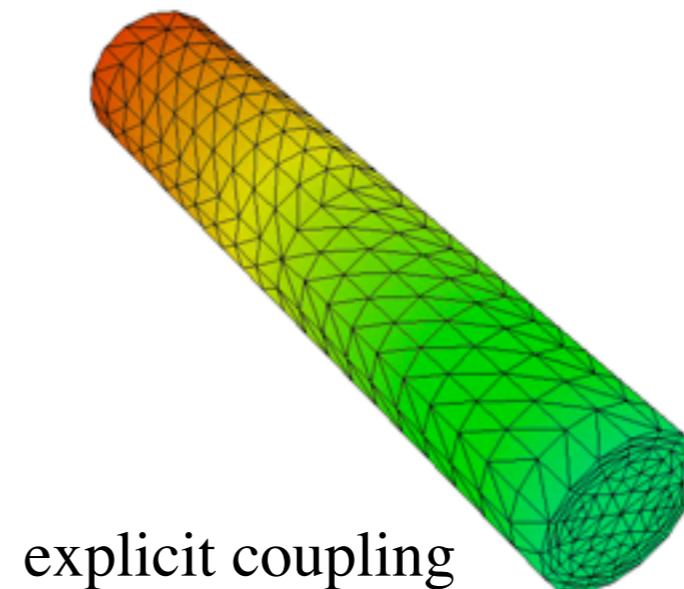
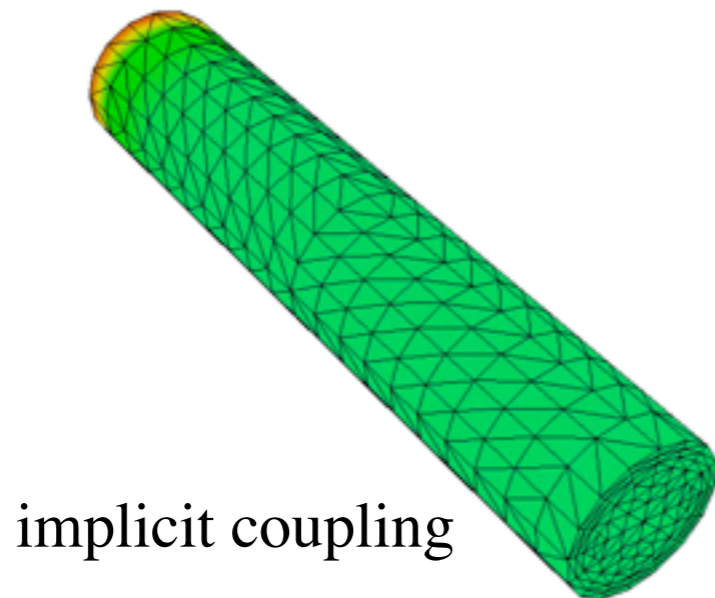
- **Explicit** scheme : one iteration Fluid/Structure at each time step
- **Implicit** scheme : many Fluid/Structure subiterations at each time step

# Explicit coupling: some observations

- Explicit algorithms are a priori very efficient:

$$\text{FSI cost} \approx \text{FLUID cost} + \text{SOLID cost}$$

- ... but naive Dirichlet-Neumann iterations are unstable !



- Explicit coupling is stable and widely used in aeroelasticity !
- Empirical observations for explicit coupling in blood flows:
  - ➔ Instabilities disappear when the solid density is (artificially) increased
  - ➔ Instabilities are independent of the time step
  - ➔ The instability is sensitive to the **length** of the domain

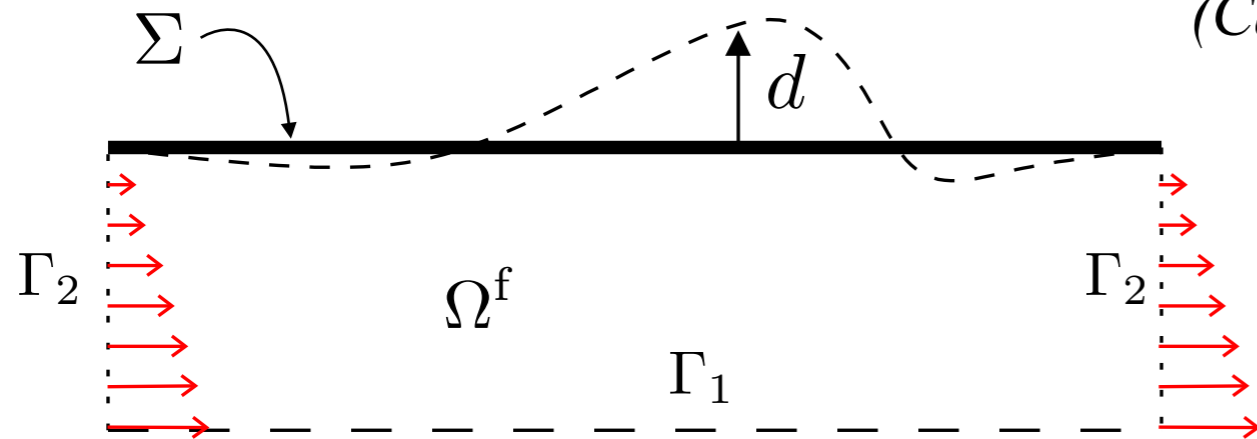
# Implicit / Explicit coupling

## Two approaches:

- Improve implicit iterations (Fixed point, Newton, ...)
  - Le Tallec-Mouro (1999) Wall-Ramm (2001), Fernández-Moubachir (2003), Matthies-Steindorf (2003), JFG-Vidrascu (2003), Mischler-van Brummelen-de Borst (2005), Deparis-Discacciati-Quarteroni (2005), Badia-Nobile-Vergara (2007), Vierendeels (2006), Vierendeels-Lanoye-Degroote-Verdonck (2007), Degroote-Annerel-Vierendeels (2010), and **many others...**
- Devise explicit coupling algorithms:
  - Projection semi-implicit coupling: Fernández-JFG-Grandmont (2007), Badia-Quaini-Quarteroni (2008)
  - Robin-Neuman : Burman-Fernández (2008)
  - Kinematically coupled time-splitting: Glowinski-Cavallini-Canic (2009), Fernández (2012)

# A 2D simplified model

(Causin, JFG, Nobile, 2005)



- **Solid:** string model (small displacements)

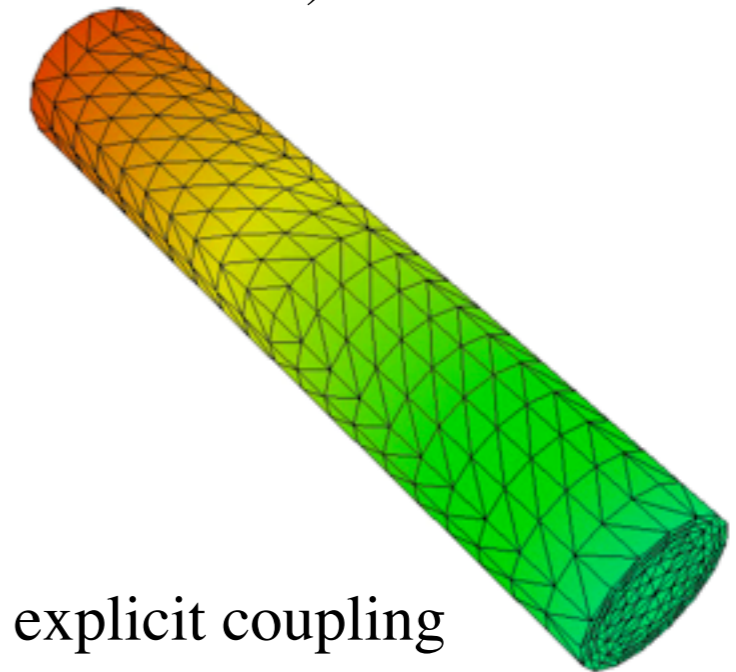
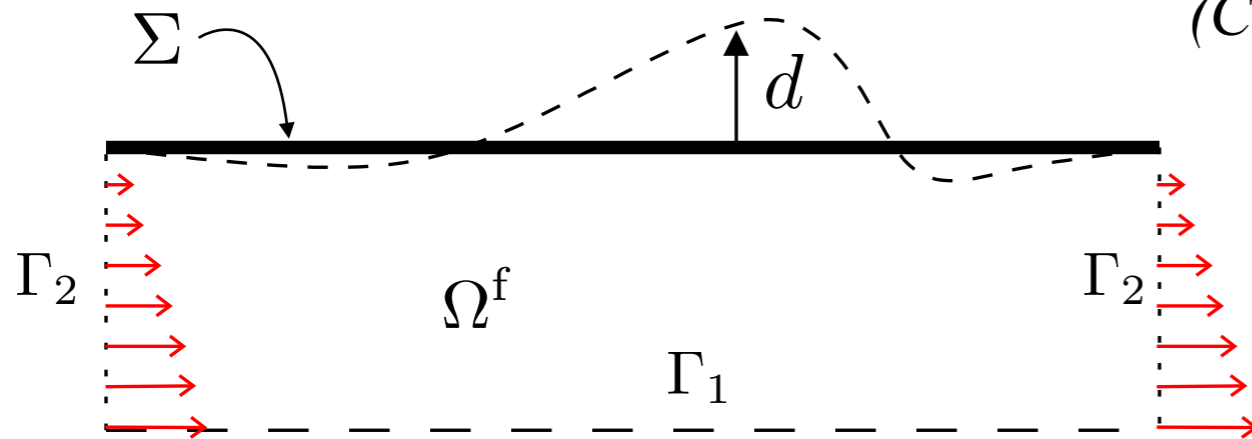
with 
$$\rho^s \varepsilon \ddot{d} + Ld = p|_{\Sigma}, \quad \text{in } \Sigma,$$

- $d$ : vertical displacement
- $\varepsilon$ : vessel thickness
- $L$ : linear operator (for instance  $L\eta = a\eta - b \frac{\partial^2 \eta}{\partial x^2}$ )



# A 2D simplified model

(Causin, JFG, Nobile, 2005)



- **Solid:** string model (infinitesimal displacements)

$$\rho^s \varepsilon \ddot{d} + Ld = p|_{\Sigma}, \quad \text{in } \Sigma,$$

- **Fluid:** fixed fluid domain, no viscous/convective terms

$$\left\{ \begin{array}{l} \rho^f \frac{\partial \mathbf{u}}{\partial t} + \nabla p = 0, \quad \text{in } \Omega^f \\ \operatorname{div} \mathbf{u} = 0, \quad \text{in } \Omega^f \\ \mathbf{u} \cdot \mathbf{n} = \dot{d}, \quad \text{on } \Sigma \\ \mathbf{u} \cdot \mathbf{n} = 0, \quad \text{on } \Gamma_1 \\ p = 0, \quad \text{on } \Gamma_2 \end{array} \right. \quad \Longrightarrow \quad \text{div} \quad \left\{ \begin{array}{l} -\Delta p = 0, \quad \text{in } \Omega^f \\ \frac{\partial p}{\partial \mathbf{n}} = -\rho^f \frac{\partial \mathbf{u}}{\partial t} \cdot \mathbf{n} = -\rho^f \ddot{d}, \quad \text{on } \Sigma \\ \frac{\partial p}{\partial \mathbf{n}} = 0, \quad \text{on } \Gamma_1 \\ p = 0 \quad \text{on } \Gamma_2 \end{array} \right.$$

- **Physics:** reproduces propagation phenomena
- **Numerics:** explicit coupling unstable

# The added-mass operator

$$\text{Fluid: } \left\{ \begin{array}{ll} -\Delta p = 0, & \text{in } \Omega^f \\ \frac{\partial p}{\partial \mathbf{n}} = -\rho^f \ddot{d}, & \text{on } \Sigma \\ \frac{\partial p}{\partial \mathbf{n}} = 0, & \text{on } \Gamma_1 \\ p = 0 & \text{on } \Gamma_2 \end{array} \right. \quad \text{Solid: } \rho^s \varepsilon \ddot{d} + Ld = p|_{\Sigma}, \quad \text{in } \Sigma,$$

## Steklov-Poincaré operator

The operator  $\mathcal{M}_A : H^{-\frac{1}{2}}(\Sigma) \rightarrow H^{\frac{1}{2}}(\Sigma)$  defined as: for each  $g \in H^{-\frac{1}{2}}(\Sigma)$  we set  $\mathcal{M}_A(g) \stackrel{\text{def}}{=} q|_{\Gamma^w}$ , where  $q \in H^1(\Omega^f)$  solves

$$\left\{ \begin{array}{ll} -\Delta q = 0, & \text{in } \Omega^f \\ \frac{\partial q}{\partial \mathbf{n}} = g, & \text{on } \Sigma \\ \frac{\partial q}{\partial \mathbf{n}} = 0, & \text{on } \Gamma_1 \\ q = 0, & \text{on } \Gamma_2 \end{array} \right.$$

is a linear, compact, positive and self-adjoint operator in  $L^2(\Sigma)$ .

From this definition, we have

$$p|_{\Sigma} = \mathcal{M}_A(-\rho^f \ddot{d}) = -\rho^f \mathcal{M}_A \ddot{d}$$

# The added-mass effect

$$\text{Fluid: } \left\{ \begin{array}{ll} -\Delta p = 0, & \text{in } \Omega^f \\ \frac{\partial p}{\partial \mathbf{n}} = -\rho^f \ddot{d}, & \text{on } \Sigma \\ \frac{\partial p}{\partial \mathbf{n}} = 0, & \text{on } \Gamma_1 \\ p = 0 & \text{on } \Gamma_2 \end{array} \right. \quad \text{Solid: } \rho^s \varepsilon \ddot{d} + Ld = p|_{\Sigma}, \quad \text{in } \Sigma, \quad (1)$$

$$p|_{\Sigma} = -\rho^f \mathcal{M}_A \ddot{d}$$

$$(\rho^s \varepsilon + \rho^f \mathcal{M}_A) \ddot{d} + Ld = 0, \quad \text{in } \Sigma \quad (2)$$

What kind of time integration scheme of (2) arises from the explicit coupling of (1) ?

# Explicit coupling and added-mass

$$\text{Fluid: } \begin{cases} \rho^f \frac{\mathbf{u}^{n+1} - \mathbf{u}^n}{\delta t} + \nabla p^{n+1} = 0 \\ \operatorname{div} \mathbf{u}^{n+1} = 0 \\ \mathbf{u}^{n+1} \cdot \mathbf{n} = \frac{d^n - d^{n-1}}{\delta t} \end{cases} \xRightarrow{\text{div}} \begin{cases} -\Delta p^{n+1} = 0 \\ \frac{\partial p^{n+1}}{\partial \mathbf{n}} = -\rho^f \frac{d^n - 2d^{n-1} + d^{n-2}}{\delta t^2} \end{cases}$$

$$\text{Solid: } \rho^s \varepsilon \frac{d^{n+1} - 2d^n + d^{n-1}}{\delta t^2} + Ld^n = p_{|\Sigma}^{n+1} \quad p_{|\Sigma}^{n+1} = -\rho^f \mathcal{M}_A \frac{d^n - 2d^{n-1} + d^{n-2}}{\delta t^2}$$

Condensed FSI problem:

$$\underbrace{\rho^s \varepsilon \frac{d^{n+1} - 2d^n + d^{n-1}}{\delta t^2}}_{\text{implicit}} + \underbrace{\rho^f \mathcal{M}_A \frac{d^n - 2d^{n-1} + d^{n-2}}{\delta t^2}}_{\text{explicit}} + Ld^n = 0$$

Explicit coupling yields an explicit discretization of the added mass

# An unconditional instability result

Proposition (*Causin-JFG-Nobile 05*)

Let  $\lambda_{\max}$  be the largest eigenvalue of  $\mathcal{M}_A$  and assume that  $L\eta = a\eta$ . Then, the previous explicit coupling scheme is **unconditionally unstable** whenever

$$\frac{\rho^f \lambda_{\max}}{\rho^s \varepsilon} \geq 1. \quad (1)$$

- ▶ The instability condition confirms the empirical observations:
  - Instabilities depend on the density ratio
  - The instability condition does not depend on the time step
  - Instabilities occur when the structure is **thin** and **slender** (**higher**  $\lambda_{\max}$  )
- ▶ Other time schemes have been considered by *Förster-Wall-Ramm 07* with analogous conclusions
- ▶ Do not forget that the first assumption to build this toy model was **incompressibility**

# Semi-implicit coupling

## Three ideas:

- ▶ Treat implicitly the added-mass effect (incompressibility, pressure stress)
- ▶ Treat explicitly the fluid domain motion, convective and viscous effects
- ▶ Perform this using a projection scheme (Chorin-Teman) within the fluid

*(Fernández, JFG, Grandmont, 2007)*

# The Chorin-Teman projection scheme

- Incompressible Navier-Stokes equations:

$$\begin{aligned} \rho^f \left( \frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right) - 2\mu \operatorname{div} \boldsymbol{\epsilon}(\mathbf{u}) + \nabla p &= \mathbf{0}, & \text{in } \Omega^f \\ \operatorname{div} \mathbf{u} &= 0, & \text{in } \Omega^f \end{aligned}$$

- **Viscous** step:

$$\begin{cases} \rho^f \left( \frac{\tilde{\mathbf{u}}^{n+1} - \mathbf{u}^n}{\delta t} + \tilde{\mathbf{u}}^{n+1} \cdot \nabla \tilde{\mathbf{u}}^{n+1} \right) - 2\mu \operatorname{div} \boldsymbol{\epsilon}(\tilde{\mathbf{u}}^{n+1}) = 0, & \text{in } \Omega \\ \tilde{\mathbf{u}}^{n+1} = 0, & \text{on } \partial\Omega \end{cases}$$

- **Projection** step:

$$\begin{cases} \rho^f \frac{\mathbf{u}^{n+1} - \tilde{\mathbf{u}}^{n+1}}{\delta t} + \nabla p^{n+1} = 0, & \text{in } \Omega \\ \operatorname{div} \mathbf{u}^{n+1} = 0, & \text{in } \Omega \\ \mathbf{u}^{n+1} \cdot \mathbf{n} = 0, & \text{on } \partial\Omega \end{cases} \implies \begin{cases} -\Delta p^{n+1} = -\frac{\rho^f}{\delta t} \operatorname{div} \tilde{\mathbf{u}}^{n+1}, & \text{in } \Omega \\ \frac{\partial p^{n+1}}{\partial \mathbf{n}} = 0, & \text{on } \partial\Omega \end{cases}$$

# Semi-implicit coupling: explicit part

- Viscous sub-step:

$$\mathbf{d}^{\text{f},n+1} = \text{Ext}(\mathbf{d}_{|\hat{\Sigma}}^n), \quad \mathbf{w}^{n+1} = \frac{\mathbf{d}^{\text{f},n+1} - \mathbf{d}^n}{\delta t}, \quad \Omega^{\text{f},n+1} = (I + \mathbf{d}^{\text{f},n+1})(\hat{\Omega}^{\text{f}}),$$

$$\rho^{\text{f}} \left( \frac{\tilde{\mathbf{u}}^{n+1} - \mathbf{u}^n}{\delta t} + (\tilde{\mathbf{u}}^{n+1} - \mathbf{w}^{n+1}) \cdot \nabla \tilde{\mathbf{u}}^{n+1} \right) - 2\mu \text{div } \boldsymbol{\epsilon}(\tilde{\mathbf{u}}^{n+1}) = 0, \quad \text{in } \Omega^{\text{f},n+1}$$
$$\tilde{\mathbf{u}}^{n+1} = \mathbf{w}^{n+1}, \quad \text{on } \Sigma^{n+1}$$

- ▶ Fluid domain, viscous and convective effects explicitly treated



# Semi-implicit coupling: implicit part

- Fluid projection sub-step (in a known domain):

$$\left\{ \begin{array}{l} \rho^f \frac{\mathbf{u}^{n+1} - \tilde{\mathbf{u}}^{n+1}}{\delta t} + \nabla p^{n+1} = 0, \quad \text{in } \Omega^{f,n+1} \\ \operatorname{div} \mathbf{u}^{n+1} = 0, \quad \text{in } \Omega^{f,n+1} \\ \mathbf{u}^{n+1} \cdot \mathbf{n} = \frac{\mathbf{d}^{n+1} - \mathbf{d}^n}{\delta t} \cdot \mathbf{n}, \quad \text{on } \Sigma^{n+1} \end{array} \right. \xRightarrow{\operatorname{div}} \left\{ \begin{array}{l} -\Delta p^{n+1} = -\frac{\rho^f}{\delta t} \operatorname{div} \tilde{\mathbf{u}}^{n+1}, \quad \text{in } \Omega^{f,n+1} \\ \frac{\partial p^{n+1}}{\partial \mathbf{n}} = -\rho^f \frac{\mathbf{d}^{n+1} - 2\mathbf{d}^n + \mathbf{d}^{n-1}}{\delta t^2}, \quad \text{on } \Sigma^{n+1} \end{array} \right.$$

- Solid equation:

$$\left\{ \begin{array}{l} \rho^s \frac{\mathbf{d}^{n+1} - 2\mathbf{d}^n + \mathbf{d}^{n-1}}{\delta t^2} - \operatorname{div} (\mathbf{F}(\mathbf{d}^{n+1}) \mathbf{S}(\mathbf{d}^{n+1})) = \mathbf{0}, \quad \text{in } \hat{\Omega}^s \\ \mathbf{F}(\mathbf{d}^{n+1}) \mathbf{S}(\mathbf{d}^{n+1}) \hat{\mathbf{n}} = J(\mathbf{d}^{f,n+1}) \boldsymbol{\sigma}(\tilde{\mathbf{u}}^{n+1}, p^{n+1}) \mathbf{F}(\mathbf{d}^{f,n+1})^{-T} \hat{\mathbf{n}}, \quad \text{on } \hat{\Sigma} \end{array} \right.$$

- ▶ Projection sub-step in a fixed fluid domain
- ▶ Implicit part solved with much cheaper inner iterations

# A stability result (linear case)

Proposition: (*Fernandez-JFG-Grandmont 2007*)

Assume the interface matching operator to be  $L^2$ -stable. Then, under condition

$$\rho^s \geq C \left( \rho^f \frac{h}{H^\alpha} + 2 \frac{\mu \delta t}{h H^\alpha} \right), \quad \text{with} \quad \alpha \stackrel{\text{def}}{=} \begin{cases} 0, & \text{if } \overline{\Omega^s} = \Sigma, \\ 1, & \text{if } \overline{\Omega^s} \neq \Sigma, \end{cases}$$

the following discrete energy inequality holds:

$$\begin{aligned} \frac{1}{\delta t} \left[ \frac{\rho^f}{2} \|\mathbf{u}_h^{n+1}\|_{0,\Omega^f}^2 - \frac{\rho^f}{2} \|\mathbf{u}_h^n\|_{0,\Omega^f}^2 + \frac{\rho^s}{2} \left\| \frac{\mathbf{d}_H^{n+1} - \mathbf{d}_H^n}{\delta t} \right\|_{0,\Omega^f}^2 - \frac{\rho^s}{2} \left\| \frac{\mathbf{d}_H^n - \mathbf{d}_H^{n-1}}{\delta t} \right\|_{0,\Omega^f}^2 \right] \\ + \frac{1}{2\delta t} [a^s(\mathbf{d}_H^{n+1}, \mathbf{d}_H^{n+1}) - a^s(\mathbf{d}_H^n, \mathbf{d}_H^n)] + \mu \|\epsilon(\tilde{\mathbf{u}}_h^{n+1})\|_{0,\Omega^f}^2 \leq 0 \end{aligned}$$

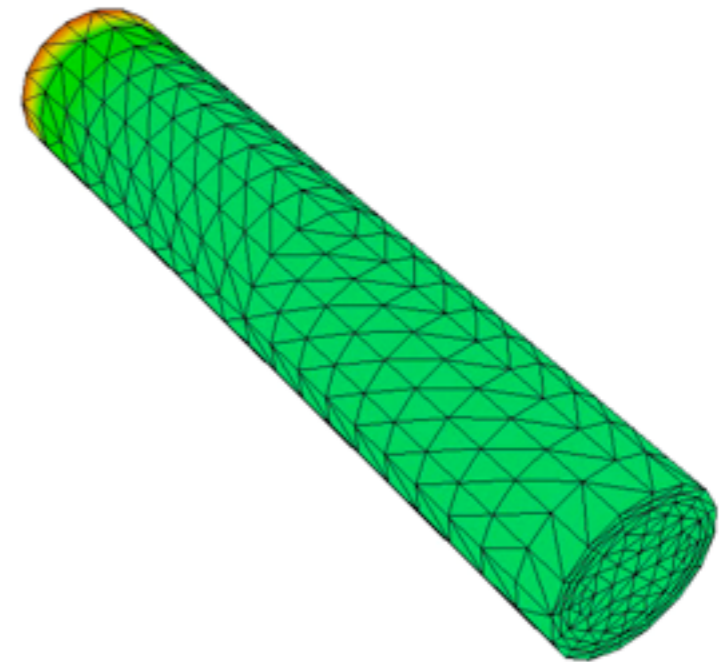
Therefore, the **semi-implicit coupling** scheme is **conditionnally stable** in the energy norm.

# Navier-Sokes / nonlinear shell coupling

- Straight cylinder: 50 time steps of length  $\delta t = 2 \times 10^{-4} s$

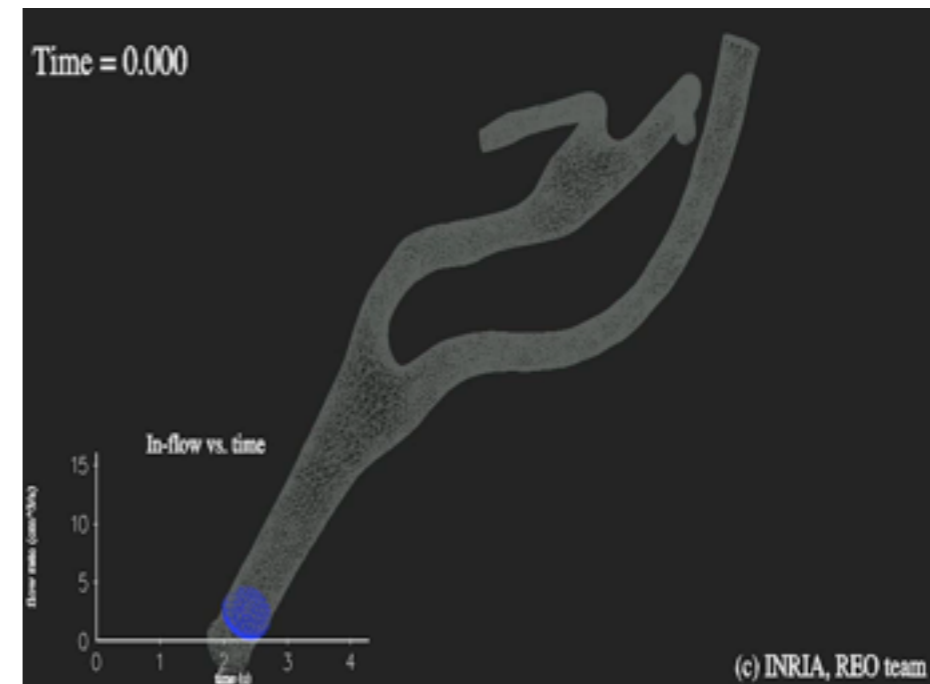
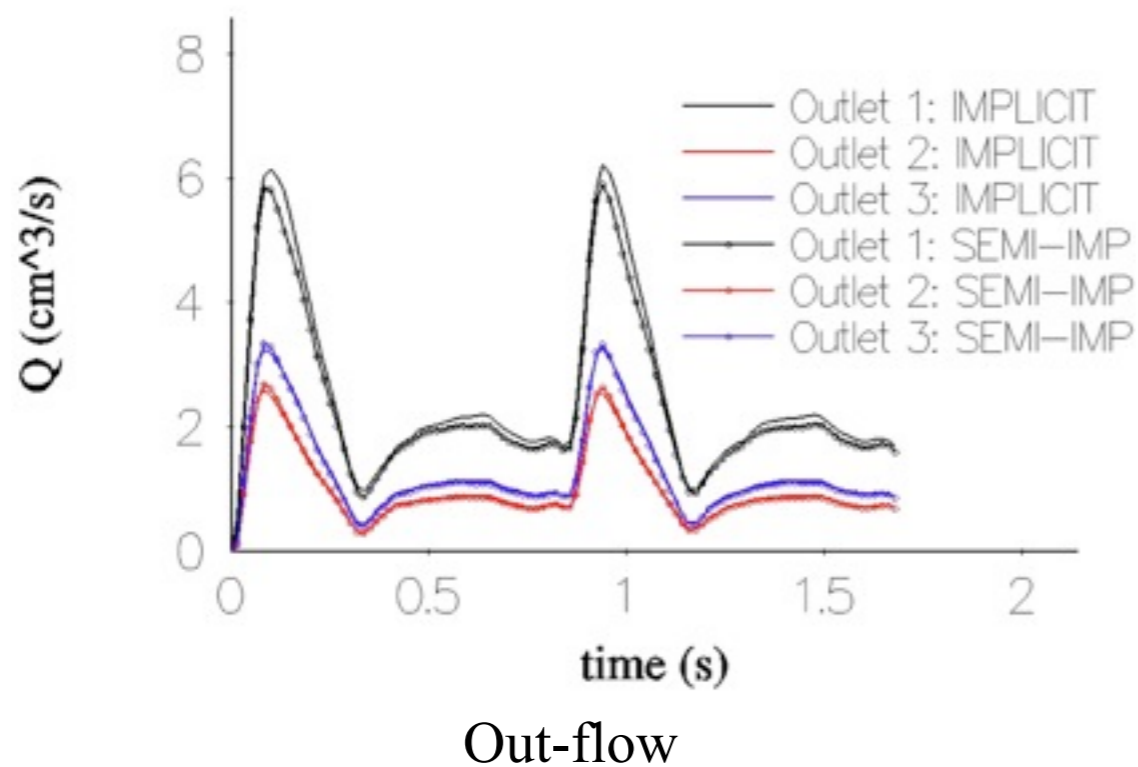
COUPLING	ALGORITHM	CPU time
Implicit	FP-Aitken	24.86
	quasi-Newton	6.05
	Newton	4.77
Semi-Implicit	Newton	1

← 2001  
← 2003  
← 2007



# Navier-Sokes / Nonlinear shell coupling

- Carotid artery (in-vivo model): 9 cardiac cycles, 4500 times steps
  - $\delta t = 1.68 \times 10^{-3} s$
  - Fluid: 70047 Tetrahedra ( $\mathbb{P}_1/\mathbb{P}_1$  FE)
  - Solid: 8103 Quadrilaterals (MITC4 FE)
  - Parameters:  $\mu = 0.035 \text{ poise}$ ,  $\rho^f = 1 \text{ g/cm}^3$ ,  
 $\rho^s = 1.2 \text{ g/cm}^3$ ,  $E = 6 \times 10^6 \text{ dynes/cm}^2$ ,  
 $\nu = 0.3$ .



COUPLING	CPU time
Implicit	<b>6.7</b>
Semi-Implicit	<b>1.0</b>

Dimensionless CPU time

# Recent approaches: explicit schemes

- Idea: only solid inertia needs to be implicitly coupled to the fluid

- Fluid

$$\left\{ \begin{array}{l} \rho^f \partial_t \mathbf{u} - \mathbf{div} \boldsymbol{\sigma}(\mathbf{u}, p) = \mathbf{0} \quad \text{in } \Omega^f \\ \mathbf{div} \mathbf{u} = 0 \quad \text{in } \Omega^f \\ \mathbf{u} = \dot{\mathbf{d}} \quad \text{on } \Sigma \end{array} \right.$$

- Thin solid

$$\left\{ \begin{array}{l} \rho^s \epsilon \partial_t \dot{\mathbf{d}} + \mathbf{L}^e \mathbf{d} = -\boldsymbol{\sigma}(\mathbf{u}, p) \mathbf{n} \quad \text{on } \Sigma \\ \dot{\mathbf{d}} = \partial_t \mathbf{d} \quad \text{on } \Sigma \end{array} \right.$$

$$\boldsymbol{\sigma}(\mathbf{u}, p) \mathbf{n} + \rho^s \epsilon \partial_t \mathbf{u} = -\mathbf{L}^e \mathbf{d} \quad \text{on } \Sigma$$

$$\boxed{\boldsymbol{\sigma}(\mathbf{u}^n, p^n) \mathbf{n} + \frac{\rho^s \epsilon}{\tau} \mathbf{u}^n = \frac{\rho^s \epsilon}{\tau} \dot{\mathbf{d}}^{n-1} - \mathbf{L}^e \mathbf{d}^*} \quad \text{on } \Sigma, \quad \mathbf{d}^* = \begin{cases} 0 \\ \mathbf{d}^{n-1} \\ \mathbf{d}^{n-1} + \tau \dot{\mathbf{d}}^{n-1} \end{cases}$$

- Added-mass free *and* parameter free
- Key issue is now the accuracy !**

# Outline

- Forward problem in Fluid-Structure Interaction
- Inverse problem in Fluid-Structure Interaction

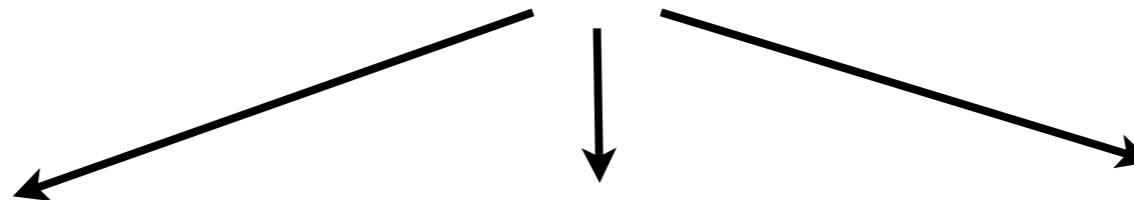
# Medical data assimilation

## Models

- Navier-Stokes equations
- Solid mechanics
- ...

## Measurements

- medical imaging (CT, MRI, ...)
- blood flow (US, PC-MRI,...)
- pressure (catheter)
- ...



## Estimate parameters

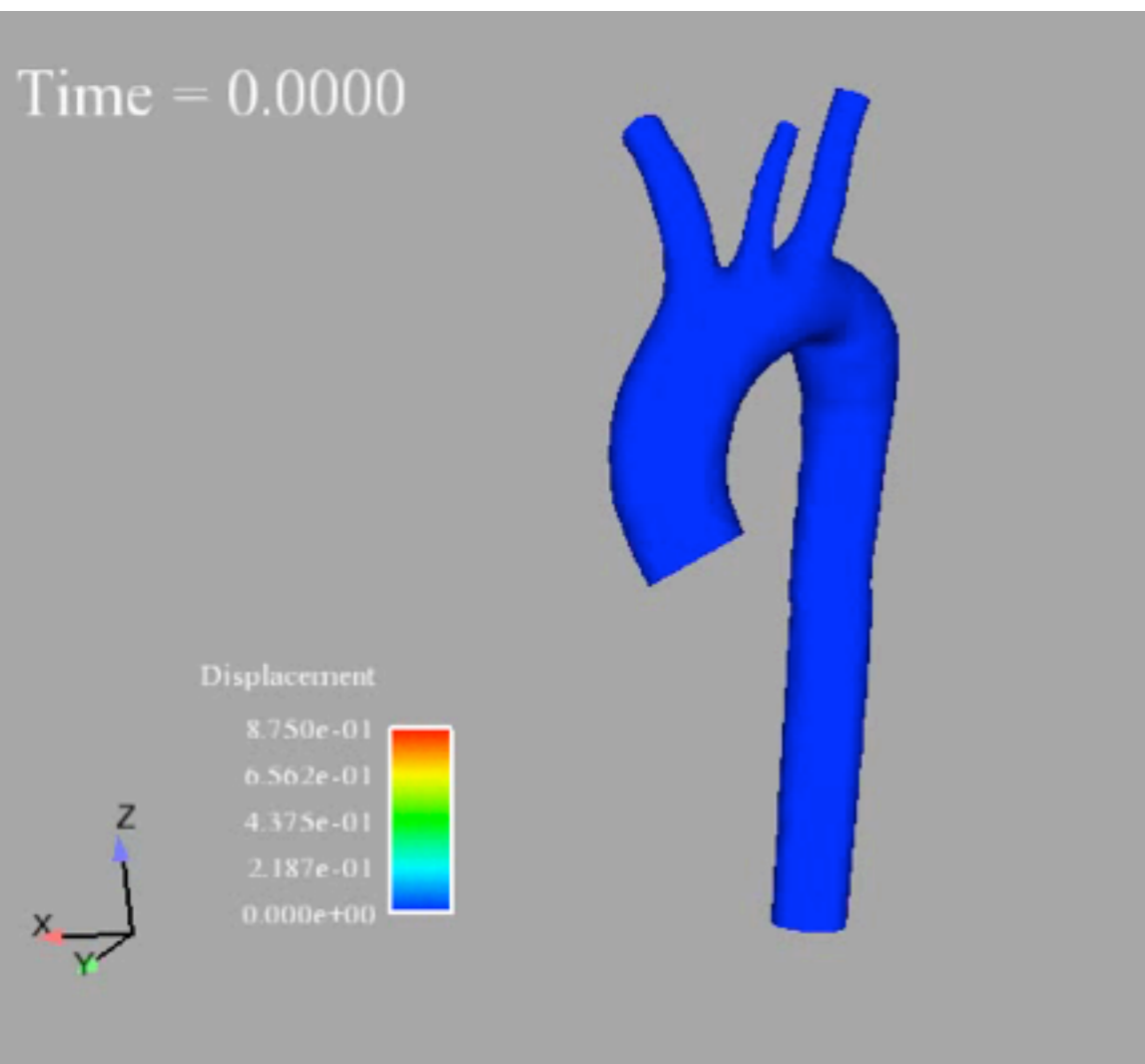
- artery wall stiffness
- boundary condition
- ...

## Access to hidden quantities

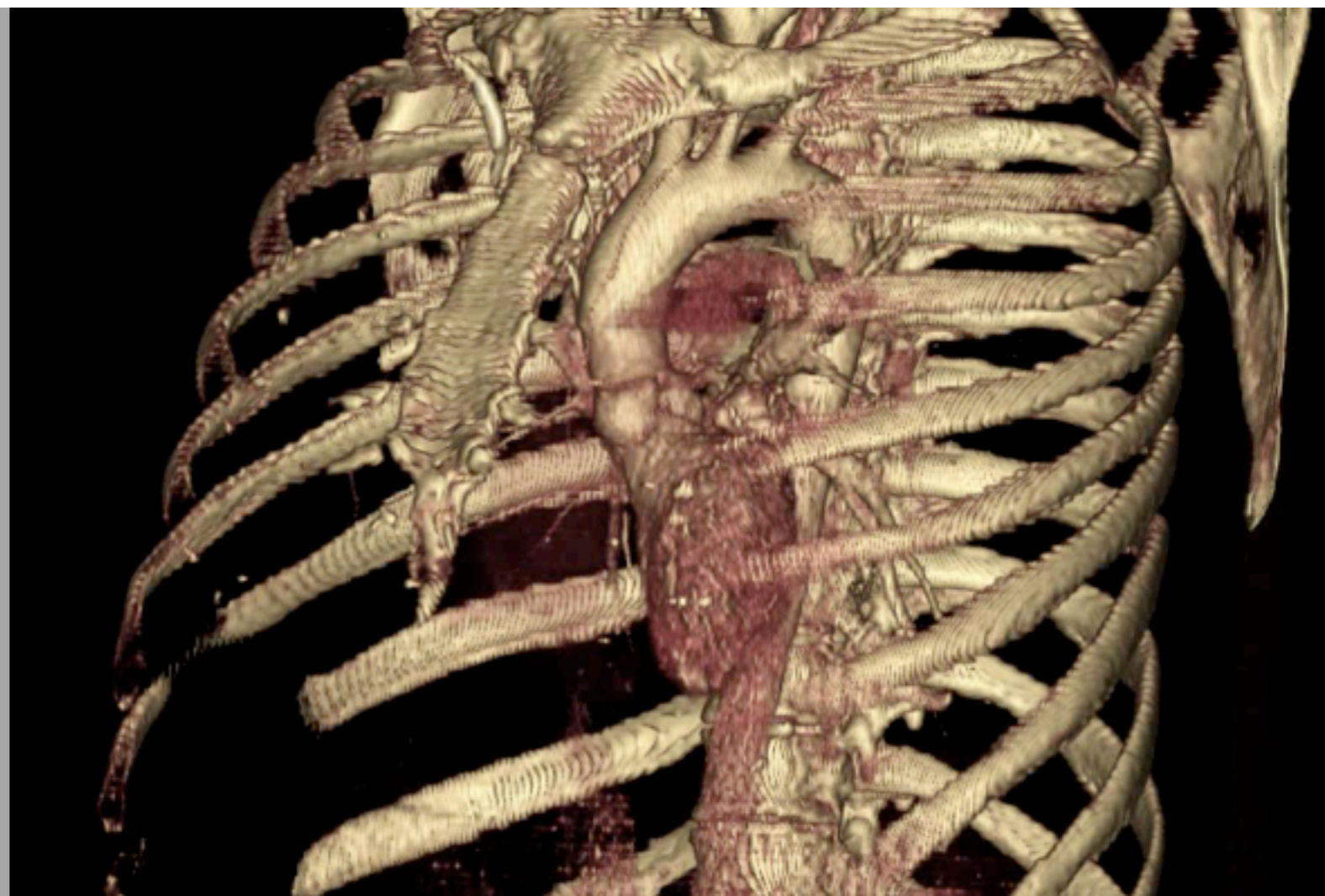
- pressure
- wall stress

## Improve measurements

- regularization
- interpolation
- ...



*INRIA*



*CVBRL, Stanford*

*Bertoglio, Chapelle, Fernandez, JFG, Moireau, 2013*  
*Moireau, Bertoglio, Xiao, Figueroa, Taylor, Chapelle, JFG, 2012*

*Bertoglio, Moireau, JFG, 2013*



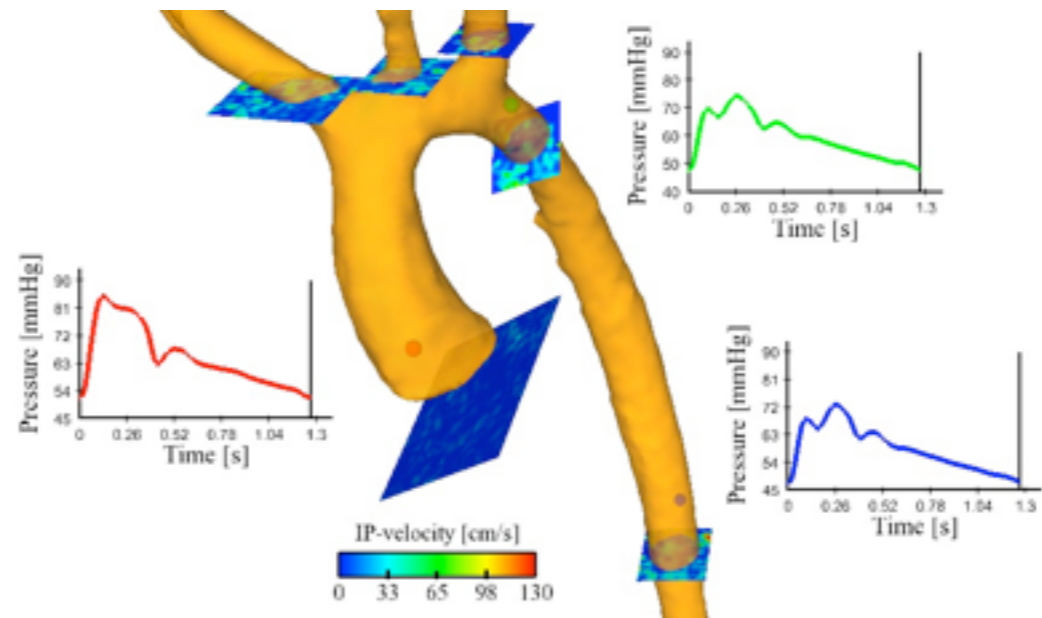
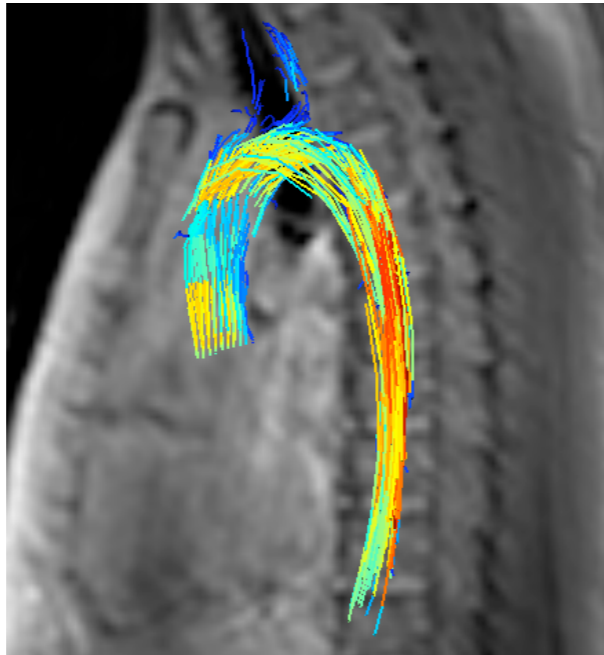
# Introduction to Luenberger observers

- Dynamical system: 
$$\begin{cases} \frac{dX}{dt} = A(X, \theta) \\ X(0) = X_0 \end{cases}$$
- Example of **state variable**:  $X = [u, d, v]$
- Example of **parameters**:  $\theta = [\text{Young modulus, boundary conditions, } \dots]$

**Imperfect** knowledge of  $X(t = 0)$  and  $\theta$ :  $\hat{X}_0$  and  $\hat{\theta}_0$

# Introduction to Luenberger observers

- Partial observations of  $X$ :  $Z = H(X)$



Data: I. Valverde, P. Beerbaum (euHeart project).

**State  
estimation**

**Parameters  
identification**

- Minimize

$$J(X_0, \theta) = \frac{1}{2} \int_0^T \|Z - H(X(t))\|_W^2 dt + \frac{1}{2} \|X_0 - \hat{X}_0\|_P^2 + \frac{1}{2} \|\theta - \hat{\theta}_0\|_P^2$$

where  $X(t)$  is the solution of the state equation associated to  $(X_0, \theta)$ .

# Data assimilation

- **Variational approach:**

- Optimization algorithms
- Usually based on gradient (adjoint equations)

In **hemodynamics**:

*Piccinelli, Mirabella, Passerini, Haber, Veneziani, 2012*

*D'Elia, Perego, Veneziani, 2012*

*Perego, Veneziani, Vergara, 2012*

- **Filtering approach:**

- Sequential correction of the state and the parameters

In **hemodynamics**:

*Moireau, Bertoglio, Xiao, Figueroa, Taylor, Chapelle, JFG, 2012*

*Bertoglio, Chapelle, Fernandez, JFG, Moireau, 2013*

*Bertoglio, Moireau, JFG, 2013*

## Strategy : reduced filtering

- Kalman filtering (**UKF**) is only used for the **parameters**  $\theta$  ( $p \ll N$ )
- A much cheaper filter (**Luenberger**) is used for the **state**  $X$

# Introduction to Luenberger observers

- In this talk: **only state estimation**

$$J(X_0) = \frac{1}{2} \int_0^T \|Z - H(X(t))\|_W^2 dt + \frac{1}{2} \|X_0 - \hat{X}_0\|_P^2$$

- In dissipative system, error in initial condition is “forgotten”....
- ... but, in view of **joint state-parameter** estimation, we want to forget it **as quickly as possible** !

# Introduction to Luenberger observers

- **Sequential estimation**

- introduce a modified system: the “**observer**”

$$\begin{cases} \frac{d\hat{X}}{dt} = A(\hat{X}) + G(Z - H(\hat{X})) \\ \hat{X}(0) = \hat{X}_0 \end{cases}$$

- with the ultimate objective to converge to the real trajectory  $X(t)$

# Introduction to Luenberger observers

- Search for the filter  $G$  such that the **optimality criterion** is satisfied:

$$X(t) = X_{[\operatorname{argmin} J(\cdot, t)]}$$

$G$  obtained from the **Riccati** or **HJB** equations.

➔ Intractable for PDEs

- Cheaper alternative:
  - renounce to the optimality criterion
  - build an *ad hoc* operator  $G$  to have the error decreased
- Idea introduced by Luenberger in 1963.
- Also known as “nudging” in the data assimilation community

Hoke-Anthes 1976, Stauffer-Seaman 1990, Auroux-Blum 2005,...

# Introduction to Luenberger observers

## Luenberger filter: looks simple but...

- Sometimes, there are pitfalls
- There is room for creativity!

## The case of a linear dynamics:

- “Real” dynamics (without noise):  $\frac{dX}{dt} = AX + G \underbrace{(Z - HX)}_{=0}$
- Observer (*Luenberger*):  $\frac{d\hat{X}}{dt} = A\hat{X} + G(Z - H\hat{X})$
- Dynamics of the **error**  $e_X = X - \hat{X}$ :

$$\frac{de_X}{dt} = (A - GH)e_X$$

# Introduction to Luenberger observers

- Spectral properties of the error dynamics:

$$(A - GH)\Phi_k = \lambda_k \Phi_k \leq 0$$

**Goal:** Devise an operator  $G$  to reduce  $\max(\operatorname{Re}(\lambda_k))$

- Typically, to decrease the initial error by a factor  $\beta$  in a time  $T_c$ :

$$\max(\operatorname{Re}(\lambda_k)) \leq \frac{\log \beta}{T_c}$$

- Ex: to have  $\beta = 10$  in  $T_c = 0.1s$ ,  $\max(\operatorname{Re}(\lambda_k)) \approx -25$



# Luenberger observers in elastodynamics

- Elastodynamics equations  $X = [d, v]$

- Velocity filtering: *Direct Velocity Feedback (DVF)*  
(Moireau-Chapelle-Le Tallec, 2008)

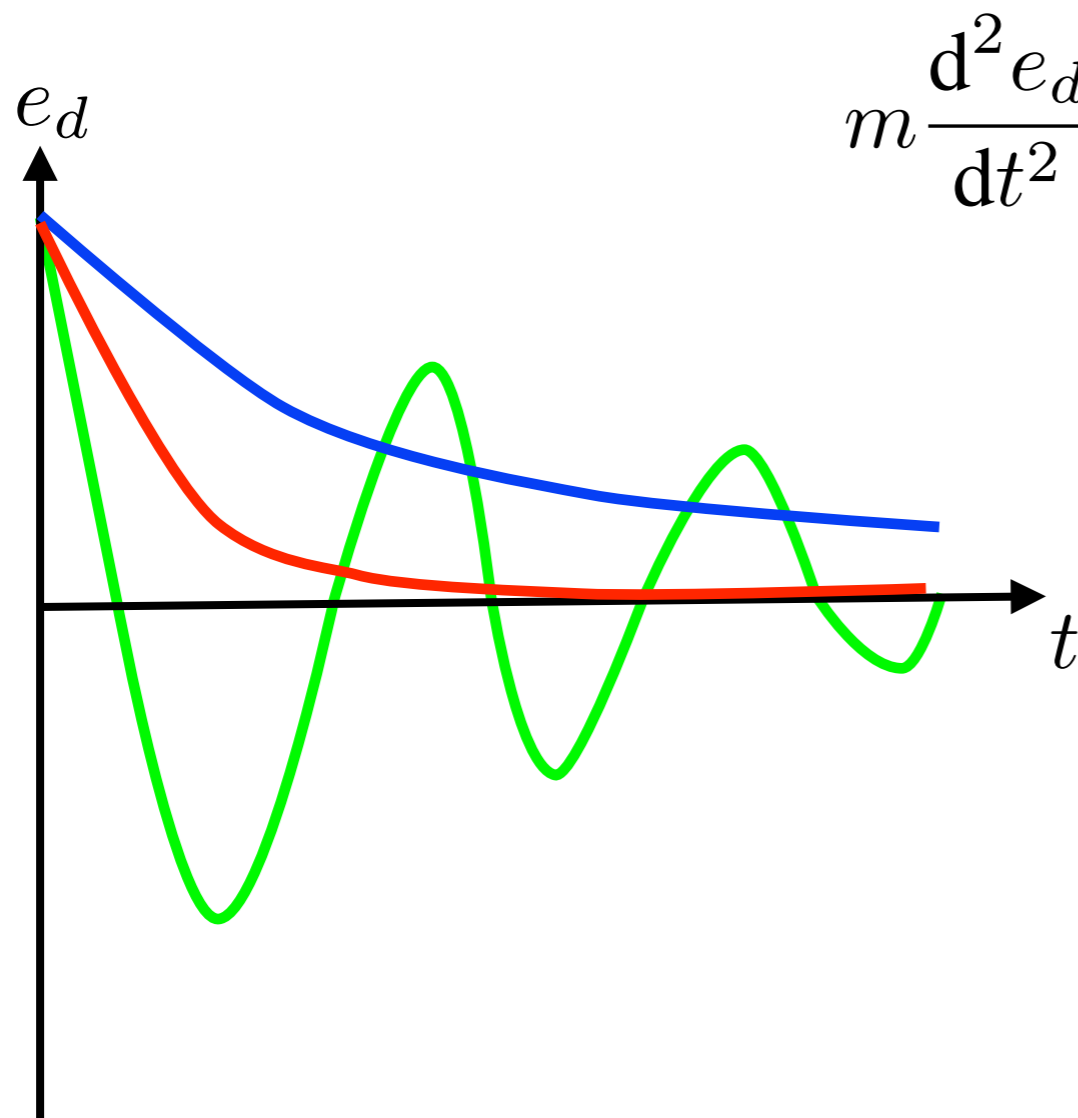
$$\int_{\Sigma_0} (z - \hat{v}) \cdot \phi_i$$

$$\begin{cases} M_s \frac{d\hat{v}}{dt} + K_s \hat{d} = R + \underbrace{\gamma_v H^T M_H (Z - H\hat{v})}_{\int_{\Sigma_0} (z - \hat{v}) \cdot \phi_i} \\ \frac{d\hat{d}}{dt} = \hat{v} \end{cases}$$

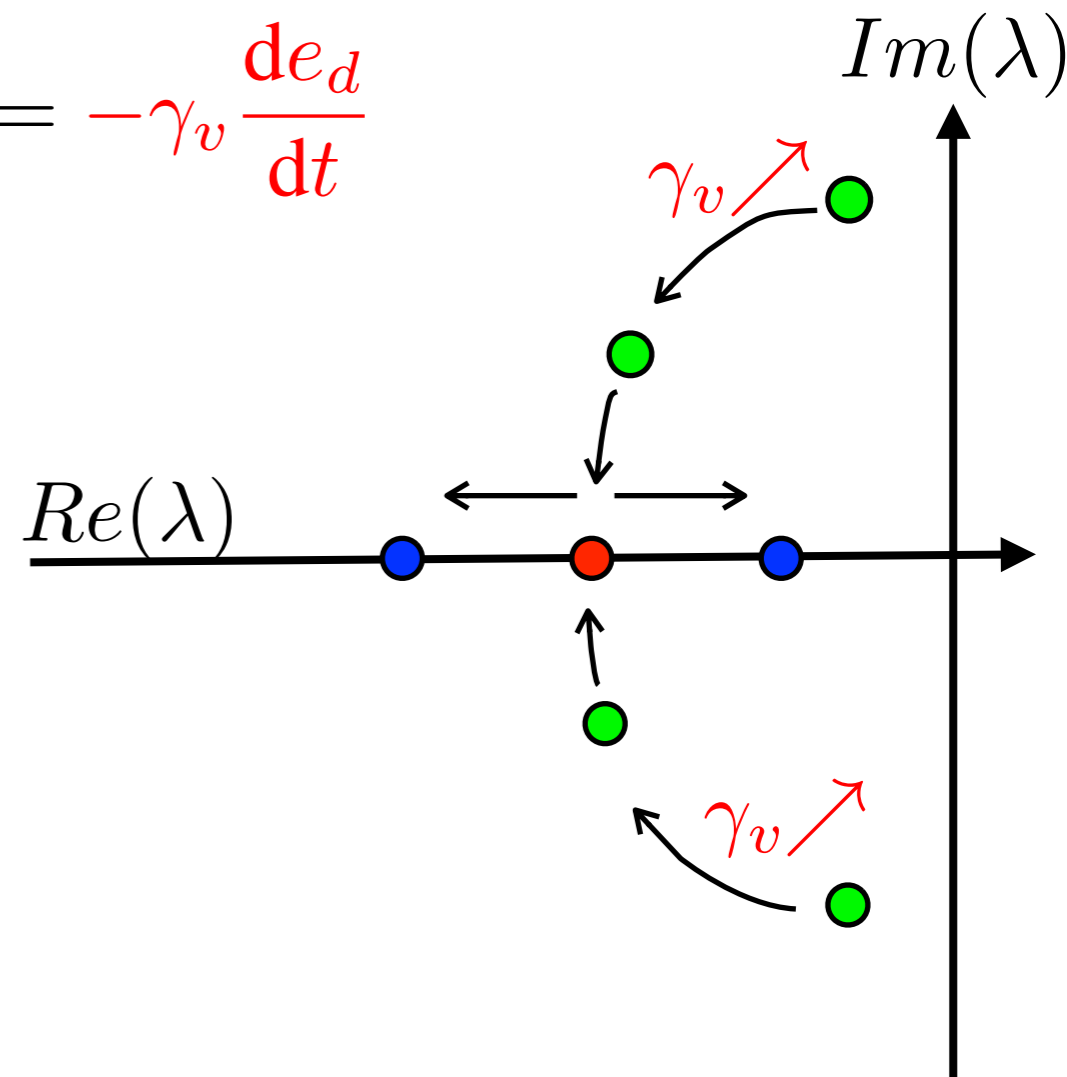
- Equation of the error:  $e_v = v - \hat{v}$ ,  $e_d = d - \hat{d}$

$$M_s \frac{de_v}{dt} + K_s e_d = -\gamma_v H^T M_H H e_v$$

- A trivial example: **linear oscillator**



$$m \frac{d^2 e_d}{dt^2} + k e_d = -\gamma_v \frac{de_d}{dt}$$



- Let  $\omega_0 = \sqrt{\frac{k}{m}}$  and  $\beta = \frac{\gamma_v}{2m}$

- If  $\beta < \omega_0$ : **underdamped**
- If  $\beta = \omega_0$ : **critically damped**
- If  $\beta > \omega_0$ : **overdamped**

# Luenberger observers in elastodynamics

- If the measurements are **displacements**
- First option:

$$\left\{ \begin{array}{l} M_s \frac{d\hat{\mathbf{v}}}{dt} + K_s \hat{\mathbf{d}} = R + \gamma_d H^T M_H (Z - H \hat{\mathbf{d}}) \\ \frac{d\hat{\mathbf{d}}}{dt} = \hat{\mathbf{v}} \end{array} \right.$$

- **Remarks:**
  - Related to the “**Image Force Method**” used in the medical imaging community
  - Poor behavior (except for systems with very large dissipation)

# Luenberger observers in elastodynamics

- Displacement filtering: *Schur Displacement Feedback (SDF)*

(Moireau-Chapelle-Le Tallec, 2009)

$$\begin{cases} M_s \frac{d\hat{\mathbf{v}}}{dt} + K_s \hat{\mathbf{d}} & = R \\ \frac{d\hat{\mathbf{d}}}{dt} & = \hat{\mathbf{v}} + \gamma_d K_\mu^{-1} H^T M_H (Z - H(\hat{\mathbf{d}})) \end{cases}$$

with  $K_\mu = K_s + \mu H^T M_\Gamma H$ .

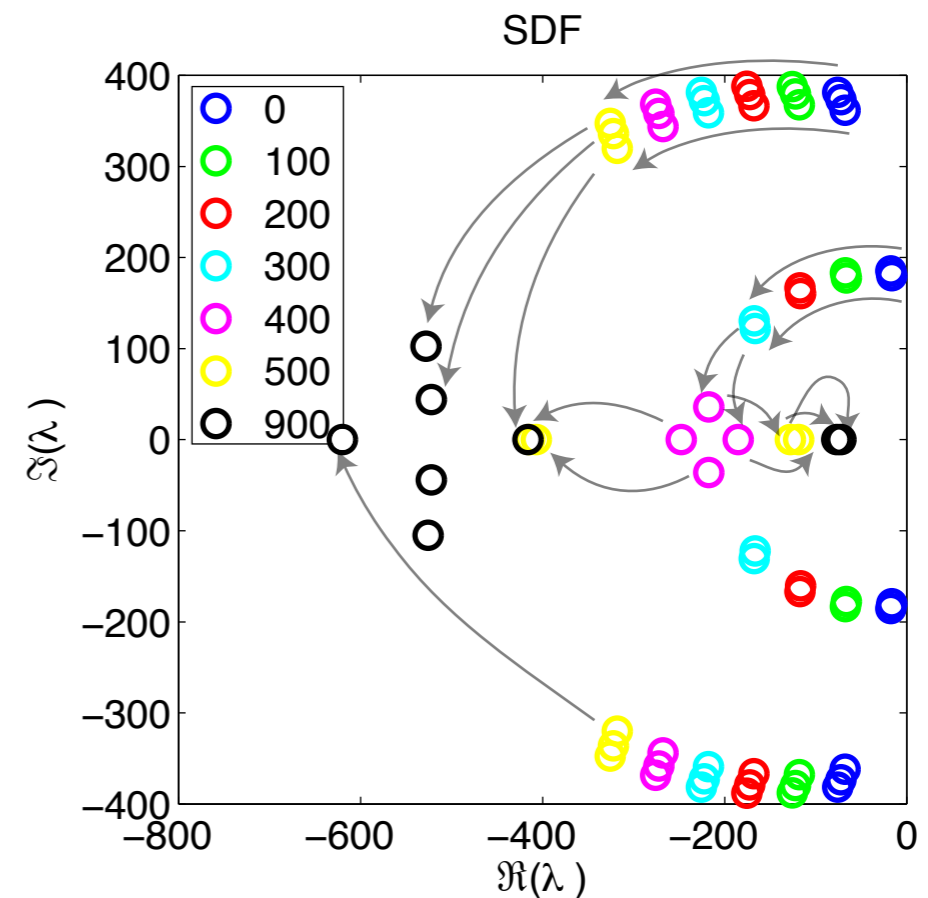
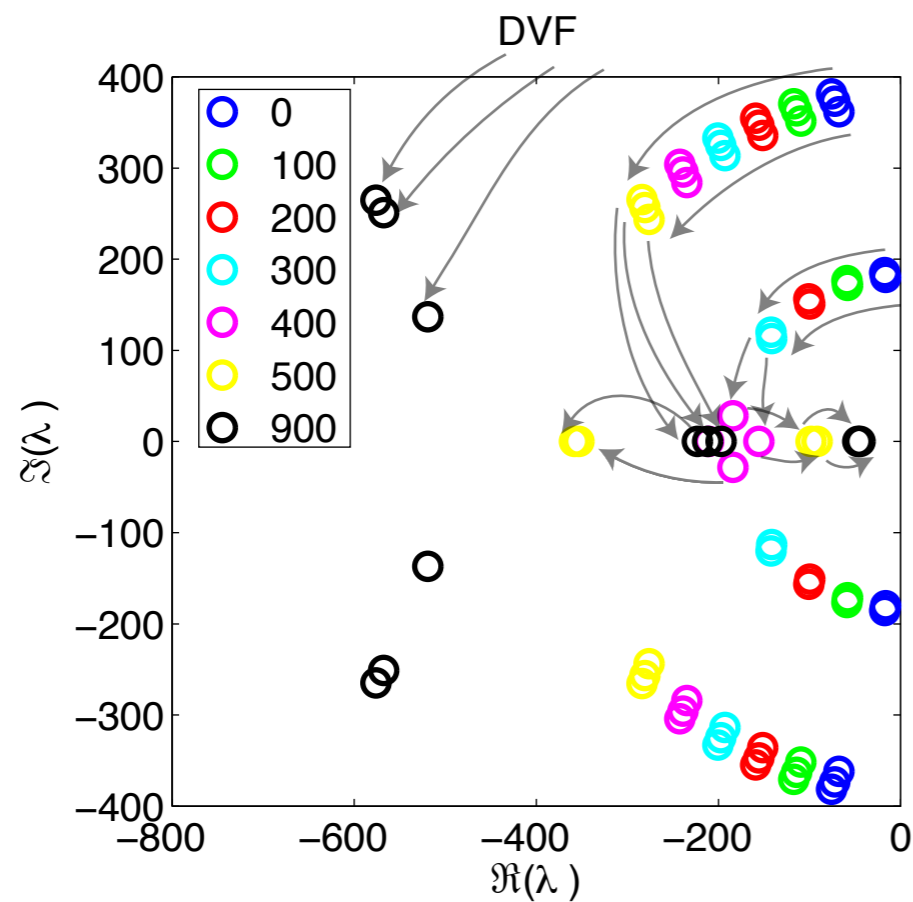
- **Remarks:**

- Velocity is no longer the derivative of displacement

$$\frac{\partial \mathbf{d}}{\partial t} = \mathbf{v} + \gamma_d \text{Ext}(\mathbf{z} - \mathbf{d})$$

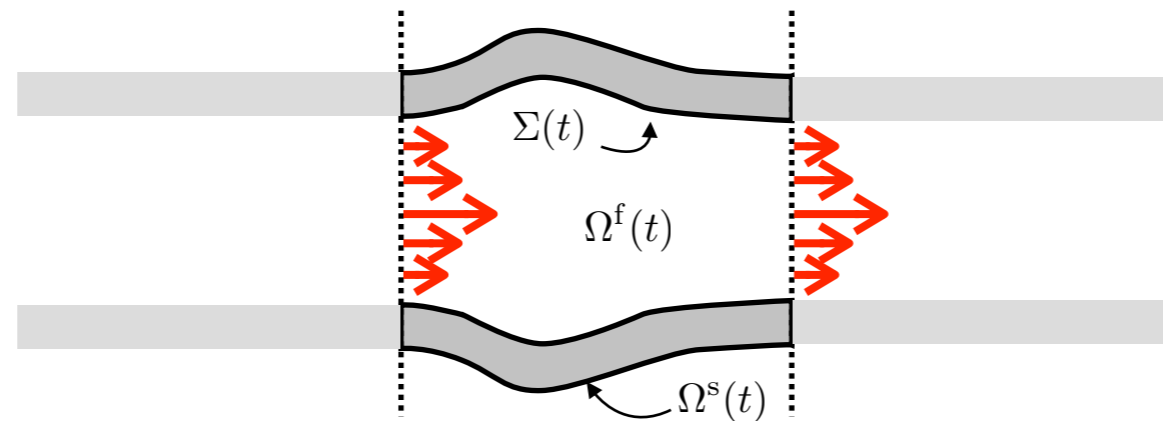
- **The norm matters!**

# Luenberger observers in elastodynamics



➔ **DVF and SDF have a similar behavior in elastodynamics**

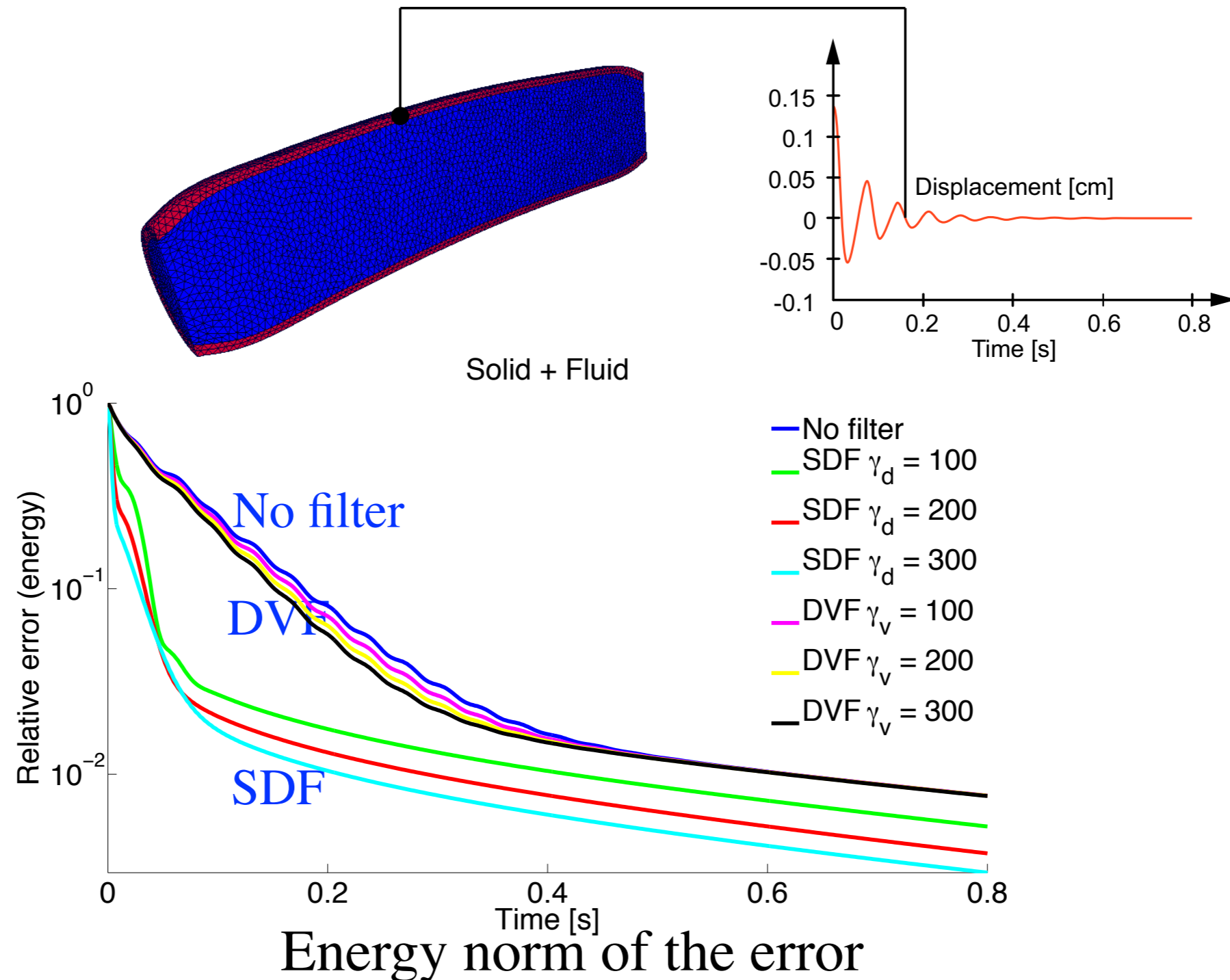
# Luenberger observers in FSI



- We limit ourselves to *solid measurements*
- We are interested in:
  - The effect of the FSI coupling
  - The effect of boundary conditions
  - The effect of fluid dissipation

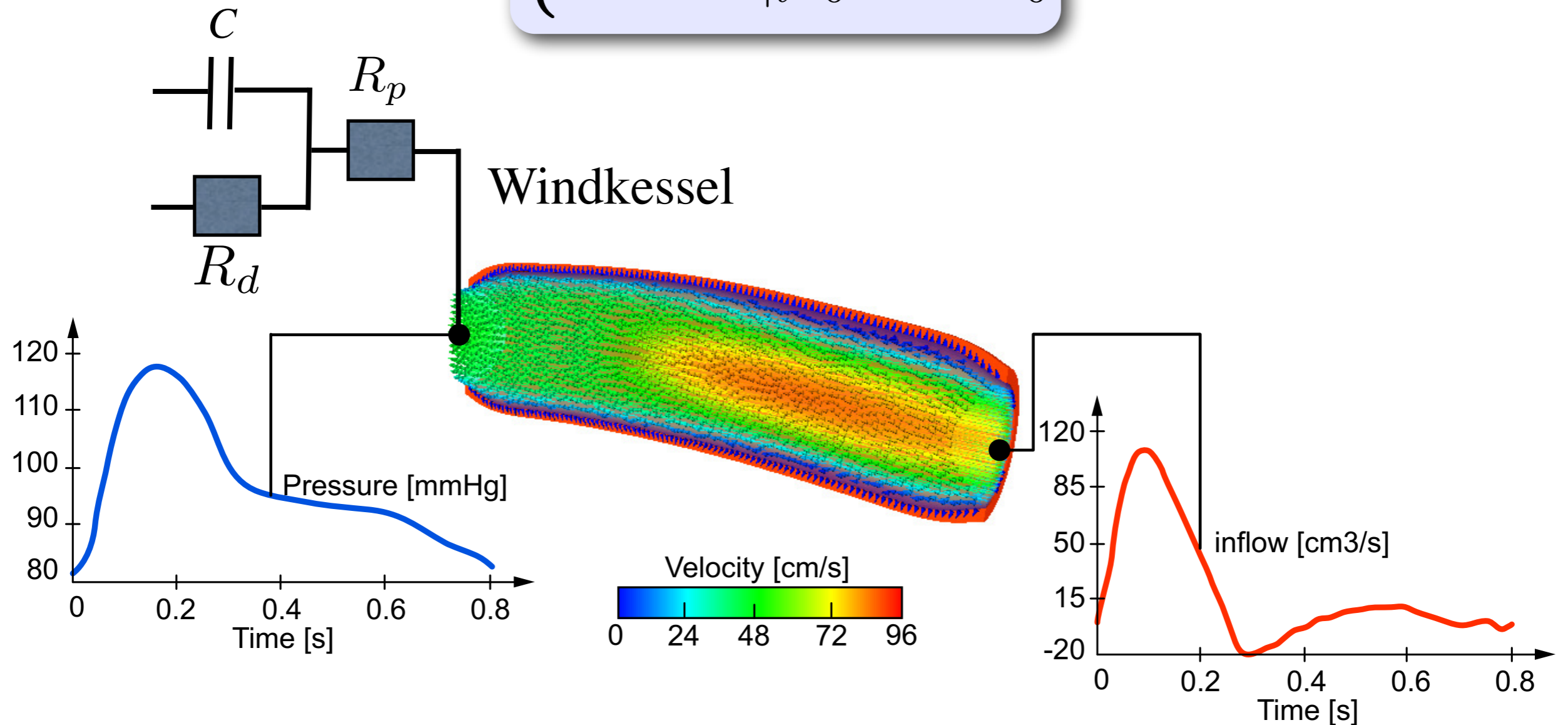
# 1st nonlinear test: stabilization to equilibrium

- Fluid initially at rest
- Initial perturbation in the solid

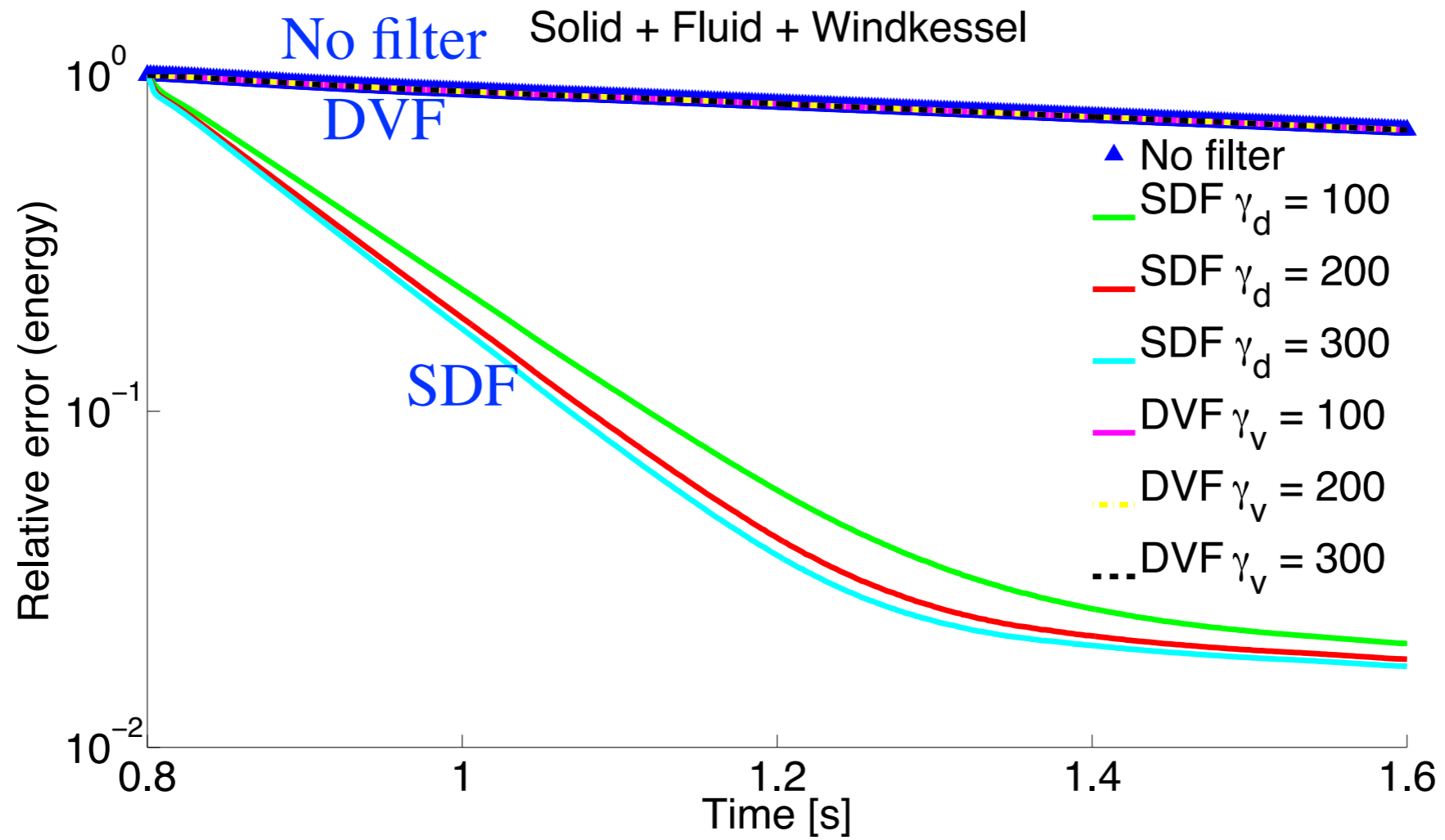


# 2d nonlinear test: hemodynamics

$p = \pi + R_p Q$  with  $\begin{cases} C \frac{d\pi}{dt} + \frac{\pi}{R_d} = Q \\ \pi|_{t=0} = \pi_0 \end{cases}$  and  $Q = \int_{\Gamma_{\text{out}}} \mathbf{u} \cdot \mathbf{n} dS$







Energy norm of the error

# SDF and DVF in FSI

## Analysis of a toy model

- Simplified fluid:

$$\left\{ \begin{array}{l} \rho^f \frac{\partial \mathbf{u}}{\partial t} + \nabla p = 0, \text{ in } \Omega^f \\ \operatorname{div} \mathbf{u} = 0, \text{ in } \Omega^f \\ \mathbf{u} \cdot \mathbf{n} = \dot{\mathbf{d}}, \text{ on } \Sigma \end{array} \right. \xRightarrow{\operatorname{div}} \left\{ \begin{array}{l} -\Delta p = 0, \text{ in } \Omega^f \\ \frac{\partial p}{\partial \mathbf{n}} = -\rho^f \frac{\partial \mathbf{u}}{\partial t} \cdot \mathbf{n} = -\rho^f \ddot{\mathbf{d}} \cdot \mathbf{n}, \text{ on } \Sigma \end{array} \right.$$

- Let  $\mathcal{M}_A$  be the “Neumann-to-Dirichlet” operator:  $p|_{\Sigma} = -\rho^f \mathcal{M}_A \ddot{\mathbf{d}} \cdot \mathbf{n}$

- Linear elasticity:

$$\left\{ \begin{array}{l} \rho^s \ddot{\mathbf{d}} - \operatorname{div} \sigma(\mathbf{d}) = 0, \text{ in } \Omega^s \\ \sigma(\mathbf{d}) \cdot \mathbf{n} = p|_{\Sigma} \mathbf{n} = -\rho^f \mathcal{M}_A \ddot{\mathbf{d}} \cdot \mathbf{n} \mathbf{n}, \text{ on } \Sigma \end{array} \right.$$

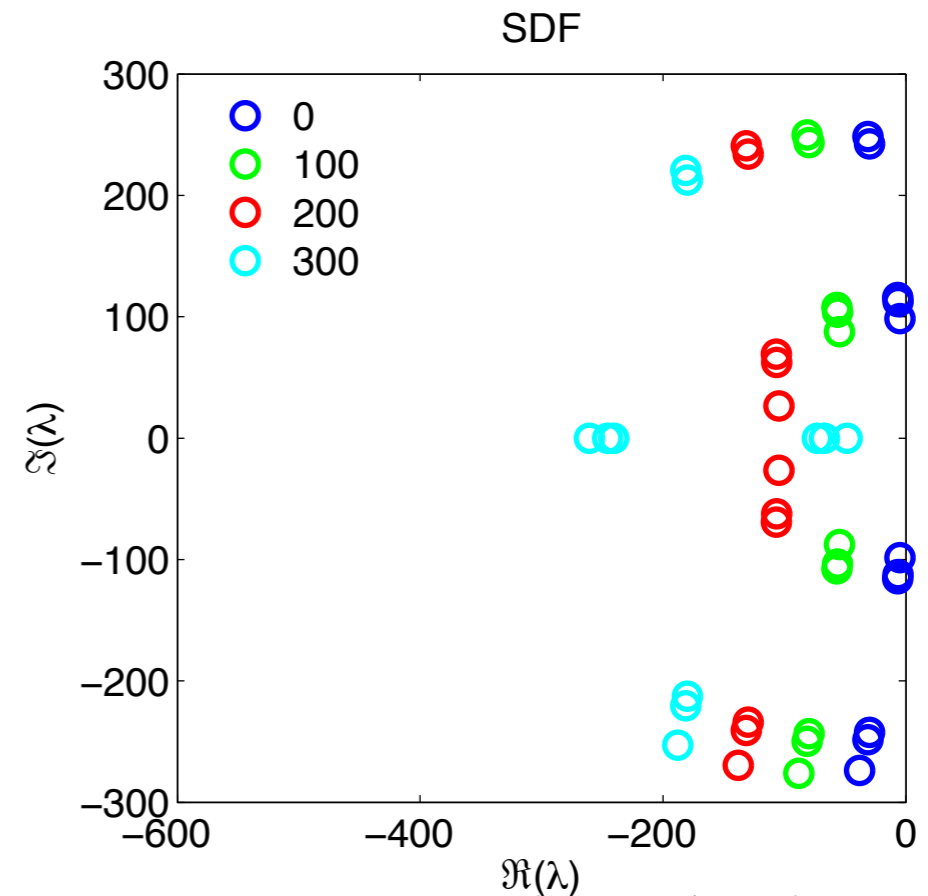
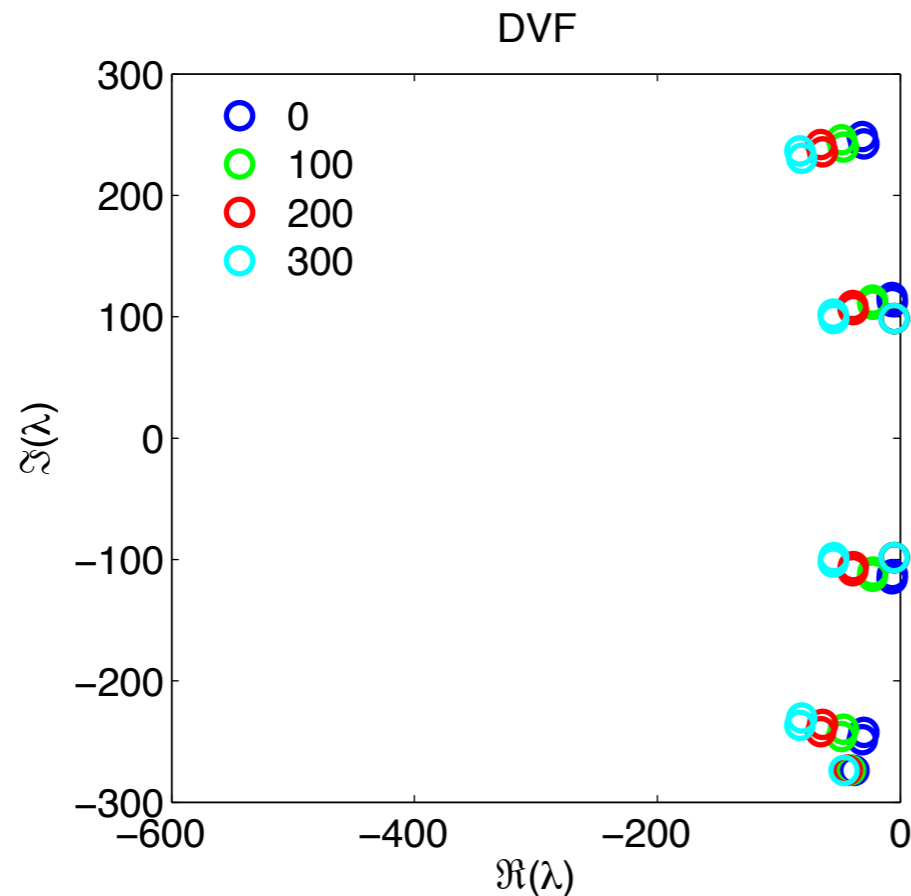
# SDF and DVF in FSI

## Analysis of a toy model

- Simplified FSI problem, with **SDF** or **DVF** **Added mass (FSI)**

$$\left\{ \begin{array}{l} (M_s + M_A) \frac{d\hat{\mathbf{v}}}{dt} + K_s \hat{\mathbf{d}} = R + \gamma_v H_v^T M_\Gamma (Z_v - H_v(\hat{\mathbf{v}})) \\ K_\mu \frac{d\hat{\mathbf{d}}}{dt} = K_\mu \hat{\mathbf{v}} + \gamma_d H_d^T M_\Gamma (Z_d - H_d(\hat{\mathbf{d}})) \end{array} \right.$$

- Evolution of  $\lambda$  for increasing  $\gamma$ :



# SDF and DVF in FSI

## Analysis of a toy model

### Sensitivity

- Let  $(\lambda(\gamma), \Phi(\gamma))$  an eigenmode. Assuming full observation:

- Velocity filter:  $\frac{\partial \lambda}{\partial \gamma_v} \Big|_{\gamma_v=0} = -\frac{1 - \Phi^T M_A \Phi}{2}$
- Displacement filter:  $\frac{\partial \lambda}{\partial \gamma_d} \Big|_{\gamma_d=0} = -\frac{1}{2}$

**Remark:** In blood flows  $\Phi^T M_A \Phi$  is close to 1

# How to improve DVF in FSI ?

➔ Change norm used to measure the discrepancy

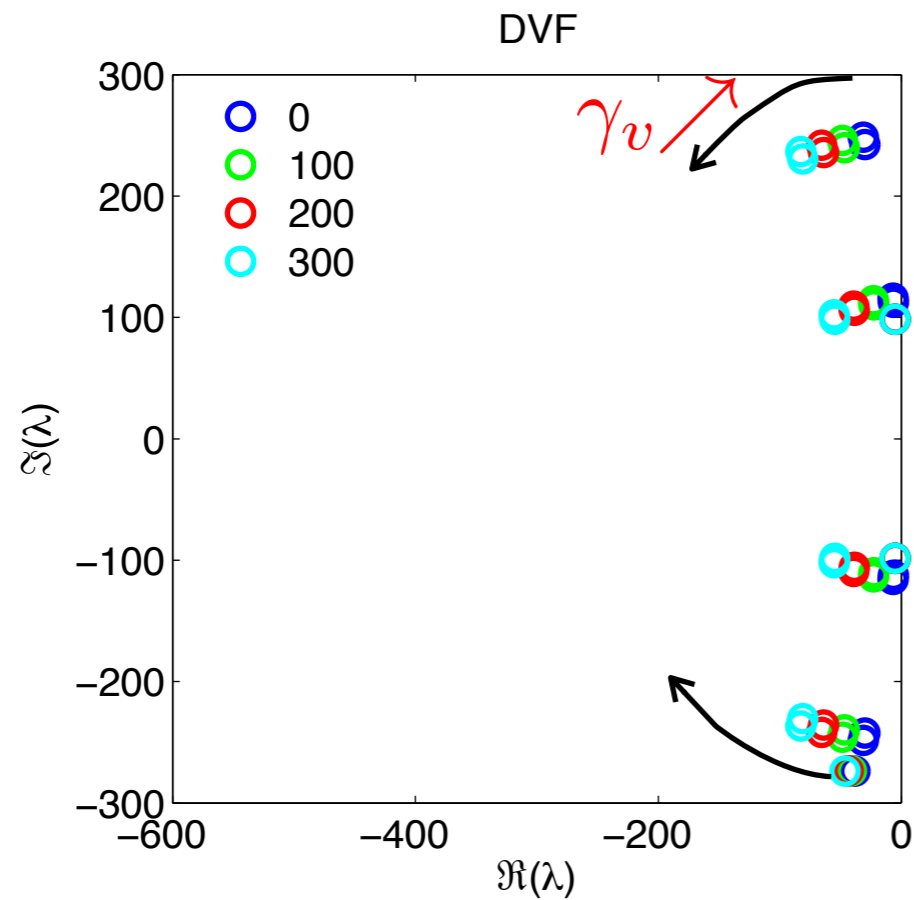
## “DVFam” filter for fluid structure problems

$$\begin{cases} M_s \frac{d\hat{\mathbf{v}}}{dt} + K_s \hat{\mathbf{d}} = R + \gamma_v H^T M_\Gamma (Z - H\hat{\mathbf{v}}) \\ \frac{d\hat{\mathbf{d}}}{dt} = \hat{\mathbf{v}} \end{cases}$$

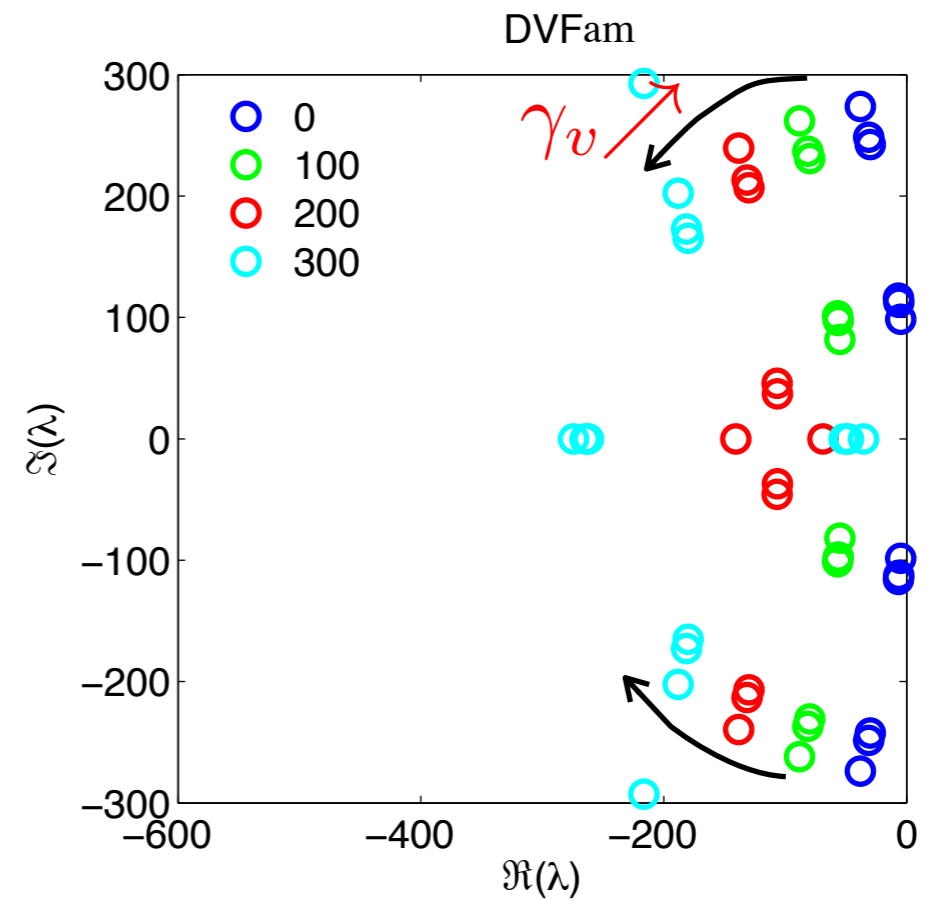
with  $M_\Gamma = M_{s,\Gamma} + M_A$ , where  $M_A$  is the added-mass operator.

➔ Then we recover  $\left. \frac{\partial \lambda}{\partial \gamma_v} \right|_{\gamma_v=0} = -\frac{1}{2}$

# Improved DVF in FSI

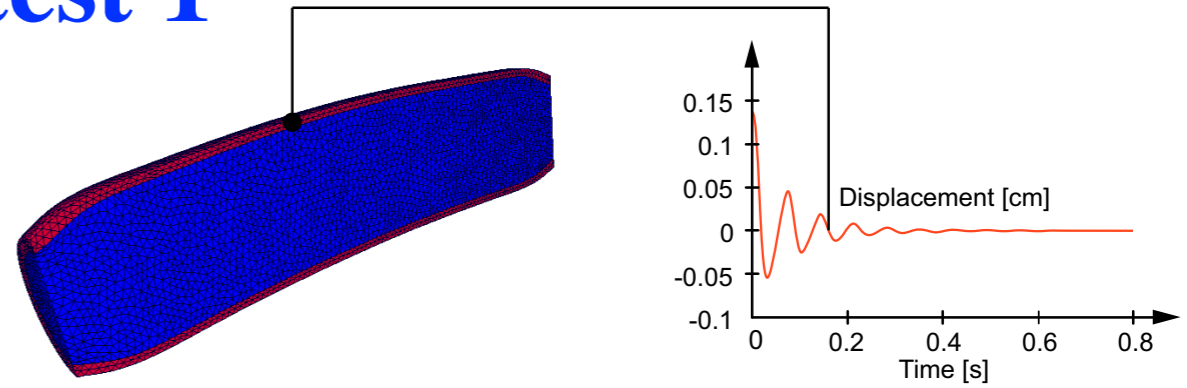


Standard DVF filter

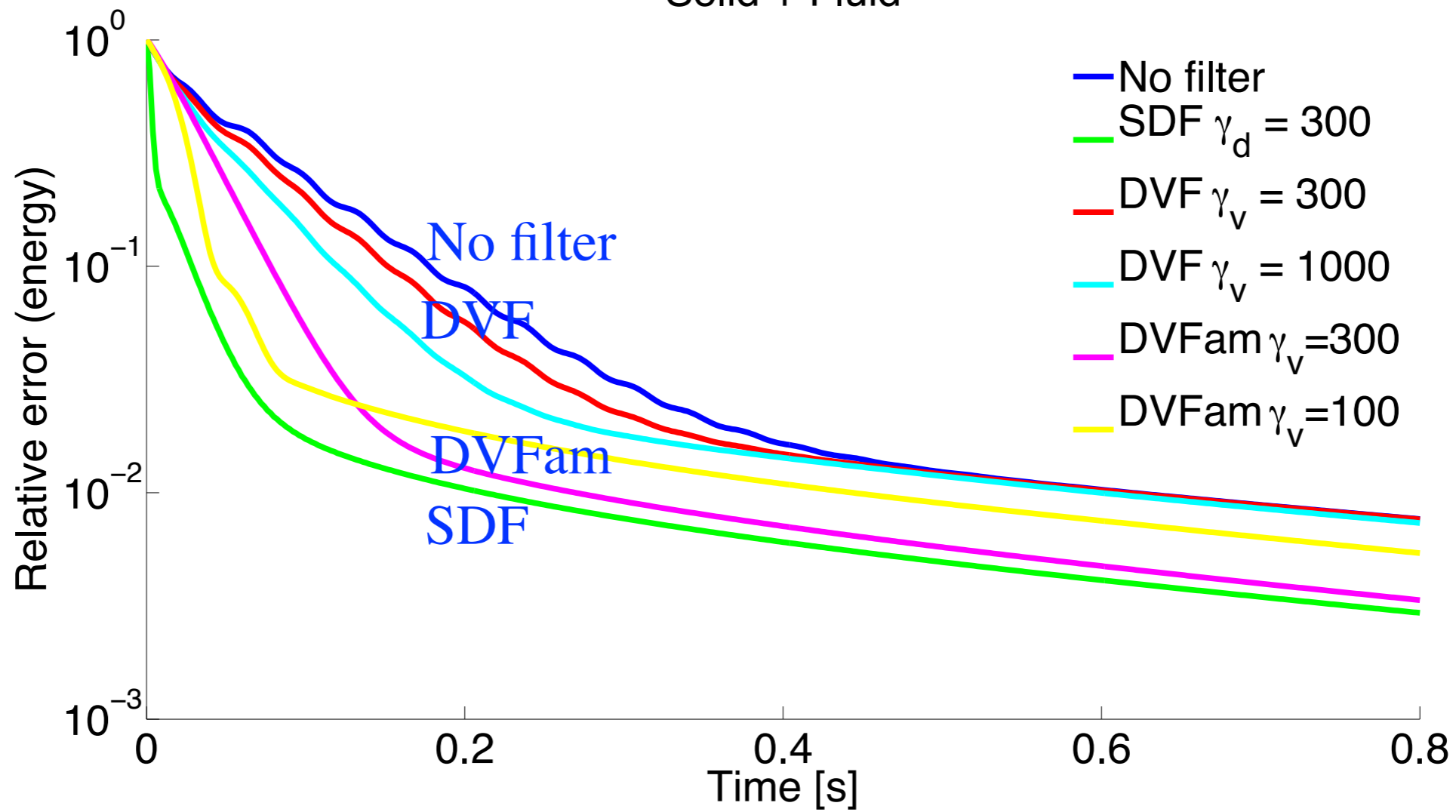


“DVFam” filter  
(norm including the added-mass)

# Application to test 1



Solid + Fluid



# Pitfall: coupling conditions

- **Reminder SDF:**  $\frac{\partial d}{\partial t} = \mathbf{v} + \gamma_d \text{Ext}(\mathbf{z} - \mathbf{d})$

Thus  $\frac{\partial d}{\partial t} \neq \mathbf{v}$  in the solid

- At the fluid-structure interface, shall we use

$$\frac{\partial d}{\partial t} = \mathbf{u} \quad \text{or} \quad \mathbf{v} = \mathbf{u} \quad ???$$

- The same analysis as before (nonlinear, spectral, sensitivity) shows that the right coupling condition is:

$$\mathbf{v} = \mathbf{u}$$


- Otherwise, it **kills** the efficiency of the SDF !



# Effect of boundary conditions

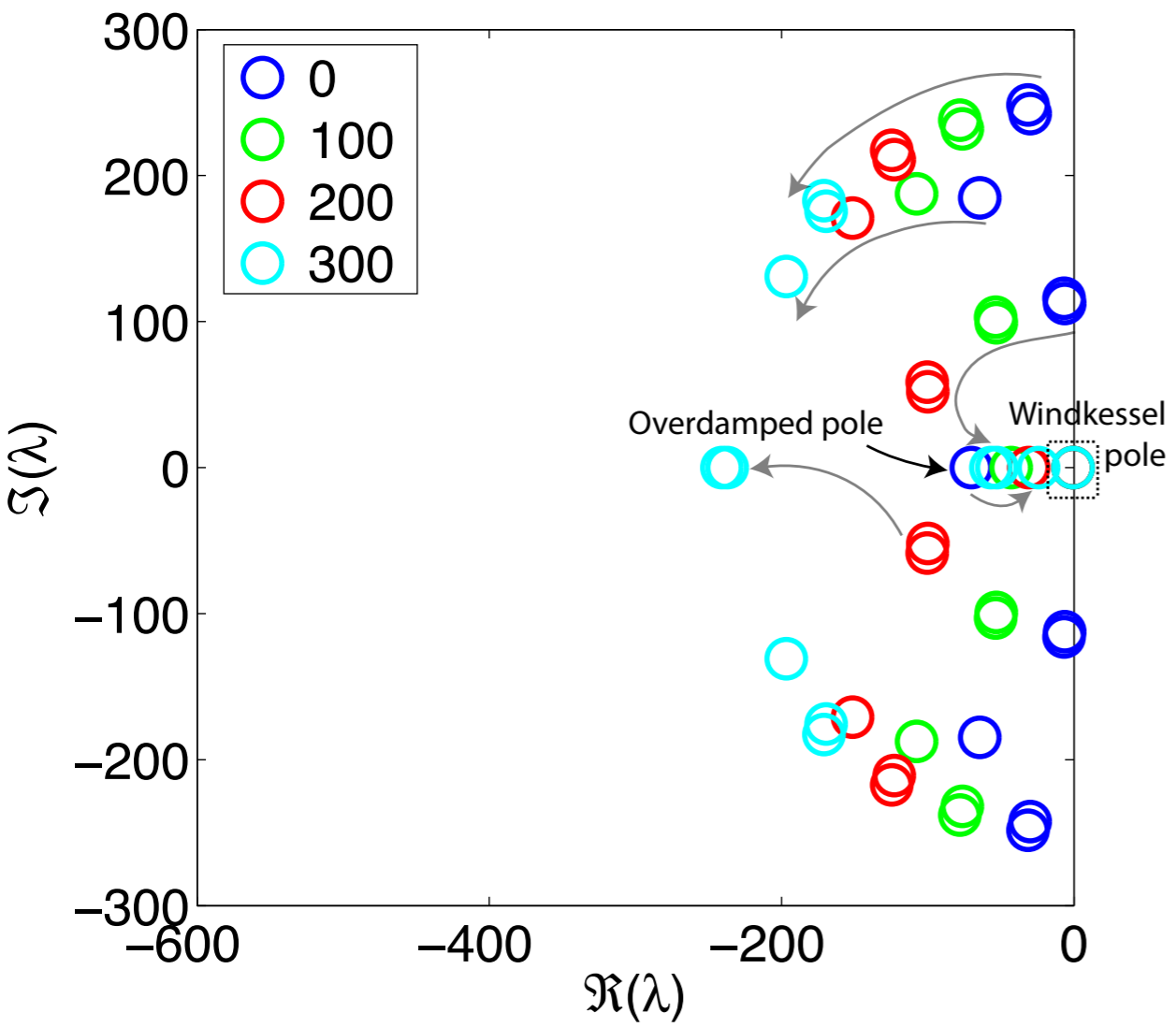
## Toy FSI model with a Windkessel Boundary Condition

$$\begin{bmatrix} K_s & 0 & 0 \\ 0 & M_s + M_A & 0 \\ 0 & 0 & C \end{bmatrix} \begin{bmatrix} \dot{Y}_s \\ \dot{U}_s \\ \dot{\pi} \end{bmatrix} = \begin{bmatrix} 0 & K_s & 0 \\ -K_s & -C_s - R_p S \cdot S^\top & S \\ 0 & -S^\top & -\frac{1}{R_d} \end{bmatrix} \begin{bmatrix} Y_s \\ U_s \\ \pi \end{bmatrix}$$

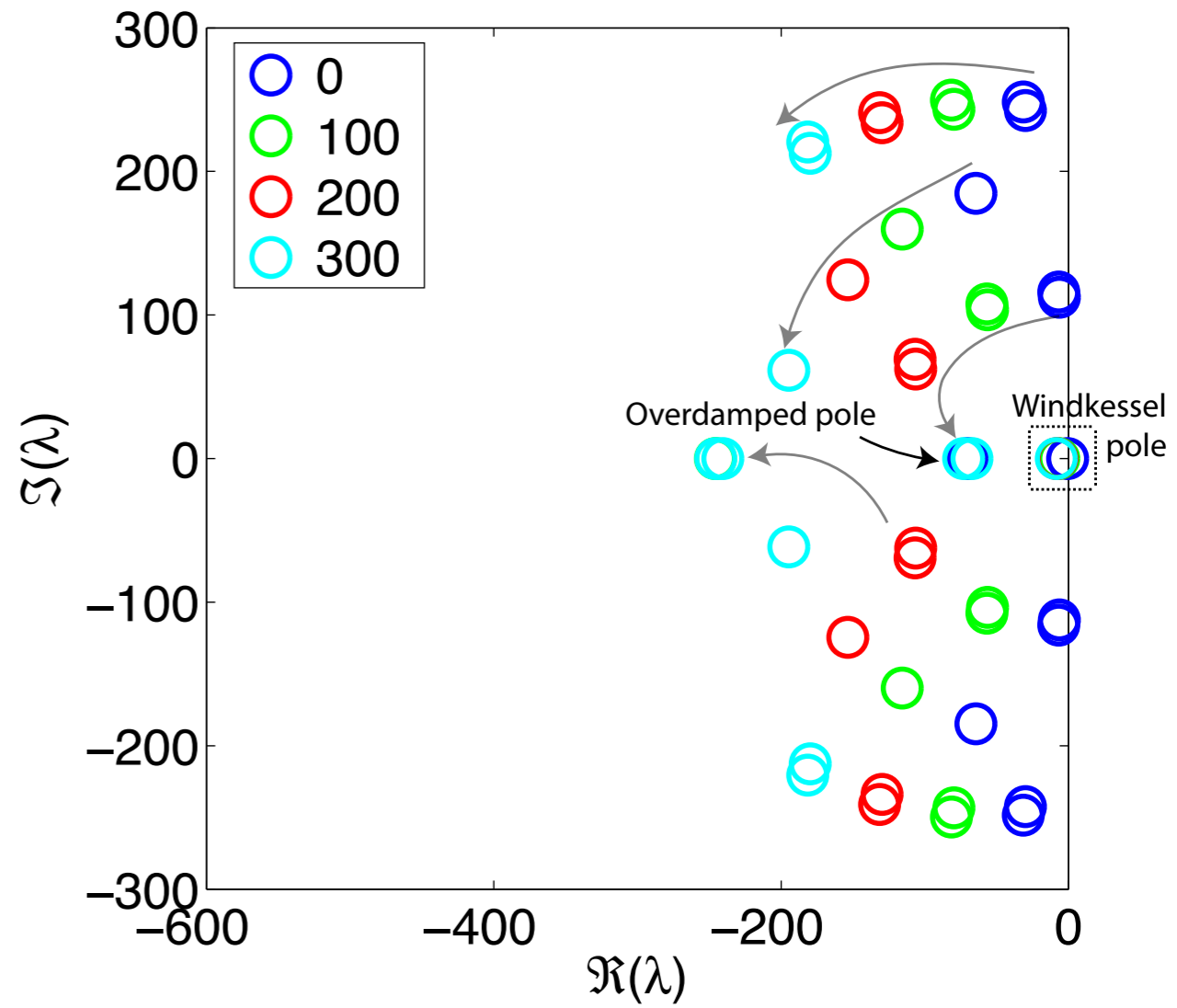

$$C \frac{d\pi}{dt} + \frac{\pi}{R_d} = Q$$

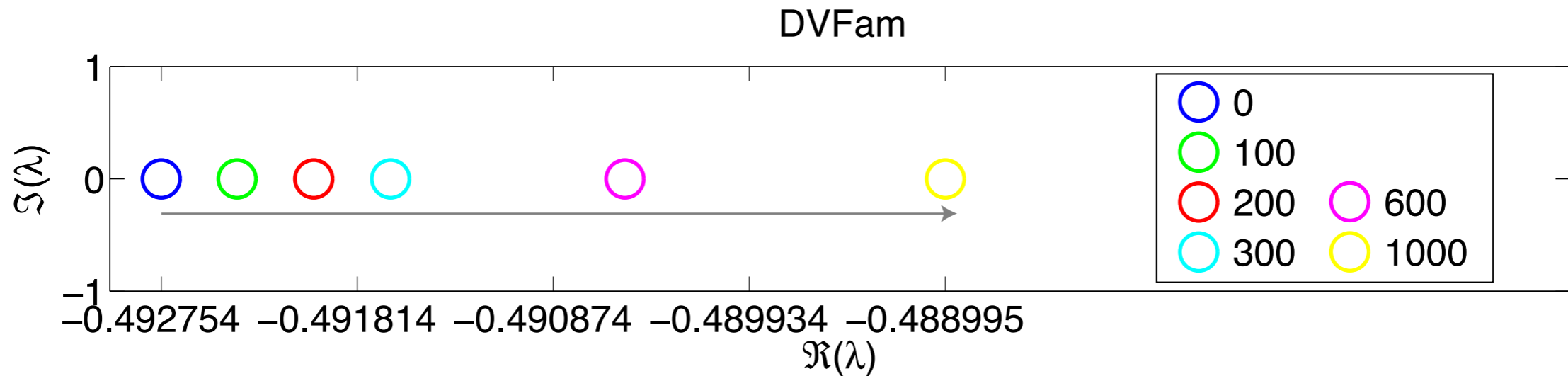
- Analytical sensitivity analysis still possible
- It confirms the observations of the numerical spectral analysis

DVFam

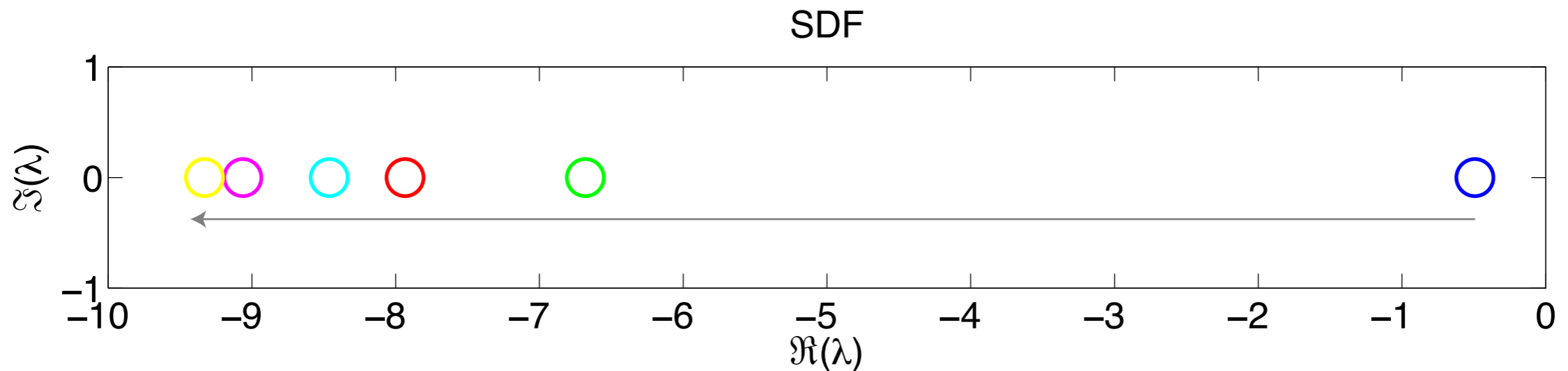


SDF





➡ DVFam (slightly) **destabilizes** the Windkessel pole



➡ SDF reasonably good at improving the Windkessel pole

# Effect of fluid dissipation

**In the toy FSI model, replace the potential fluid by Stokes:**








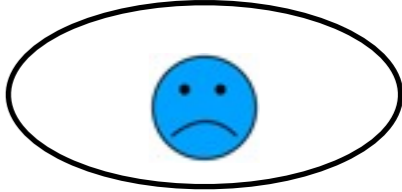
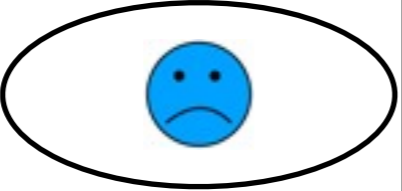



$$\begin{cases} \rho_f \partial_t \mathbf{u}_f - \nabla \cdot \boldsymbol{\sigma}_f(\mathbf{u}_f, p) = \mathbf{0}, & \text{in } \Omega_0^f \\ \nabla \cdot \mathbf{u}_f = 0, & \text{in } \Omega_0^f \end{cases}$$

- First 100 smallest eigenvalues in module :
  - Real
  - Almost the same with Stokes or with Stokes + Structure
  - Almost unaffected by any filter

# Summary

Displacement meas.

Velocity meas.

	SDF with $u=v$	SDF with $u=\dot{d}$	DVF	DVFam
Added-mass				
Dissipative BC				
Fluid viscosity				

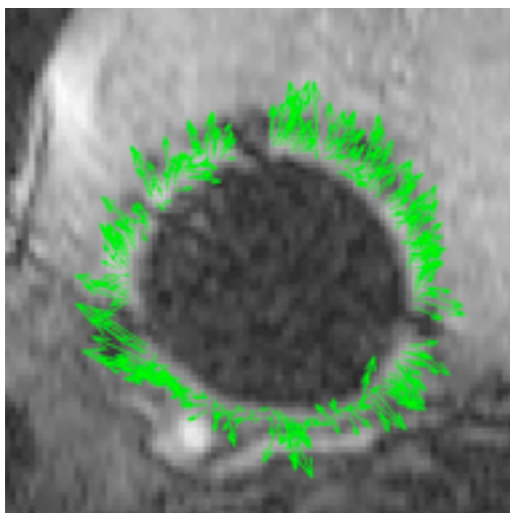
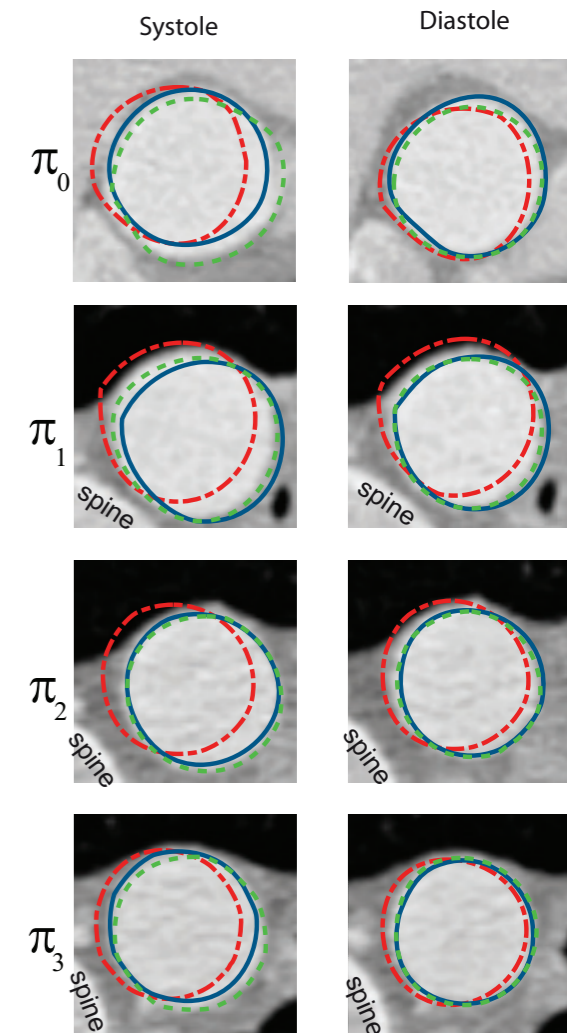
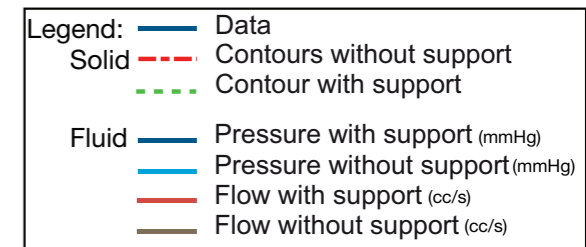
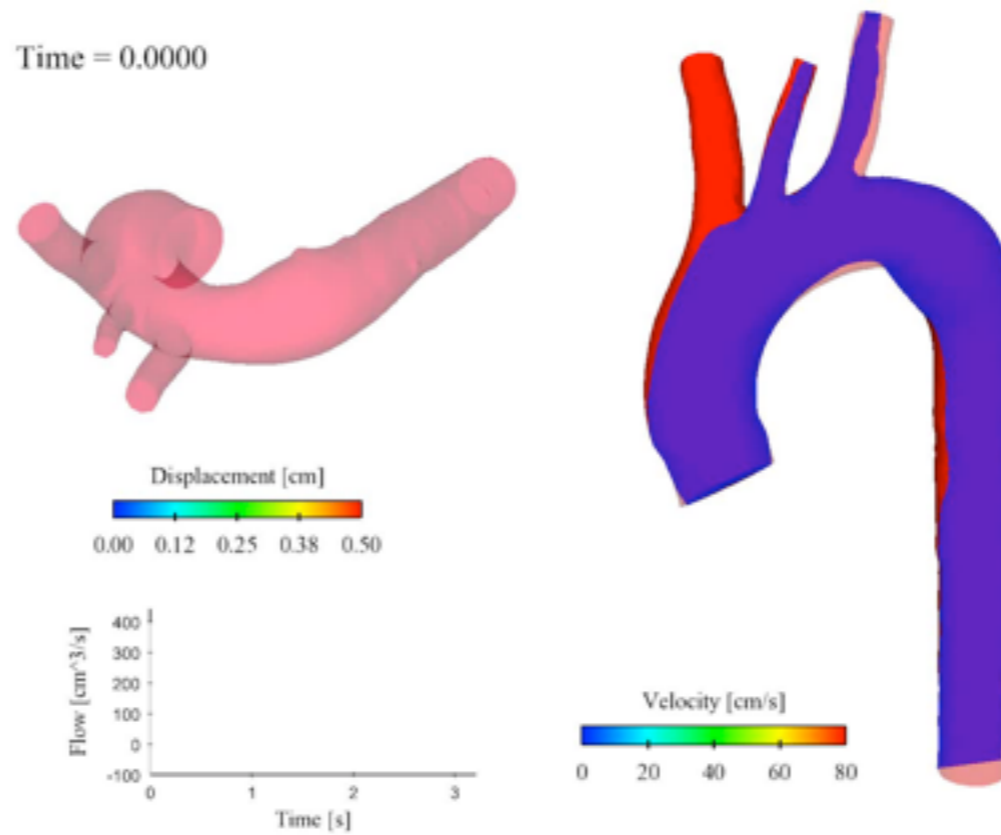
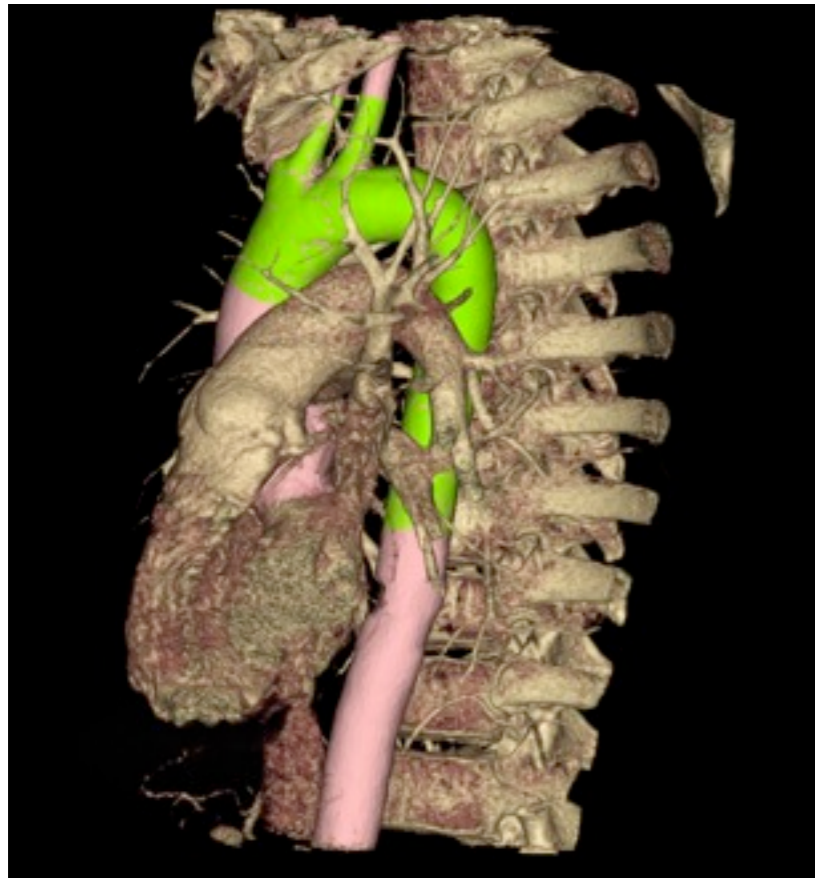
## Possible remedies

- Add pressure measurements and consider Windkessel observer like:

$$R_d C \dot{\hat{\pi}} + \hat{\pi} = R_d \hat{Q} + \gamma_{\pi} (z_{\pi} - \hat{\pi}),$$

- Add fluid measurements and devise a filter for the fluid

# Application: external tissue estimation



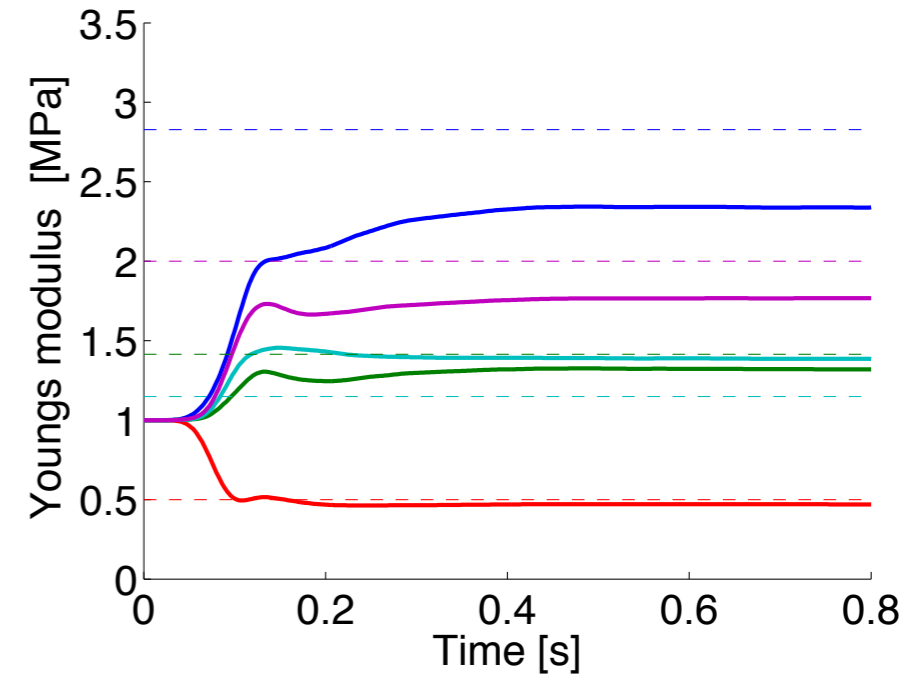
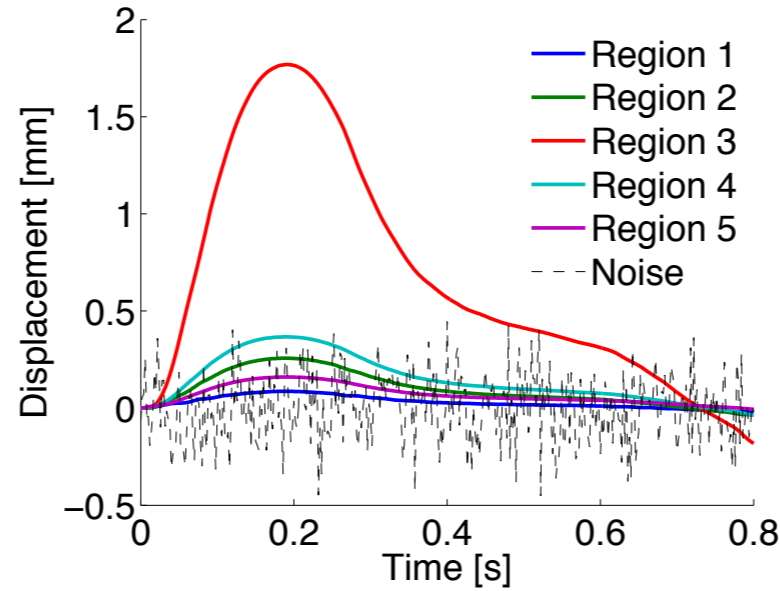
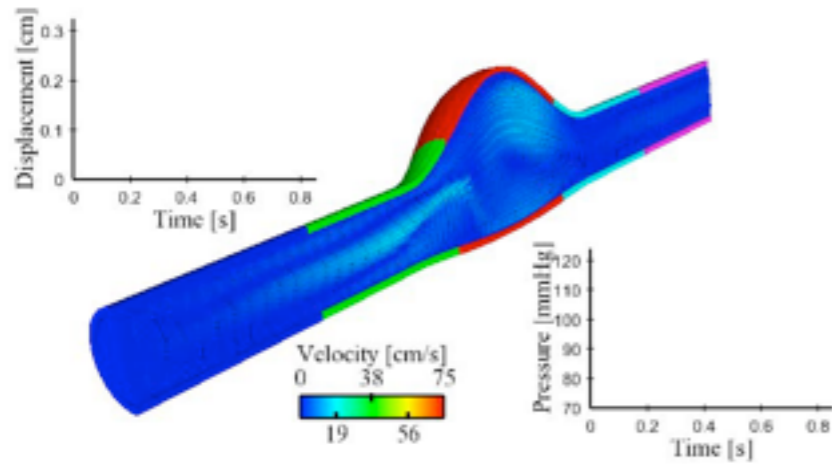
$$\sigma_s \mathbf{n} = -k_s \mathbf{d} - c_s \frac{\partial \mathbf{d}}{\partial t}$$

with heterogeneous coefficients

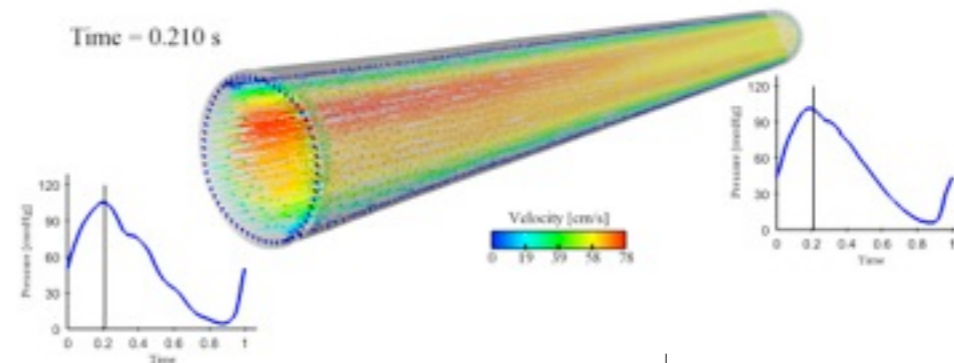
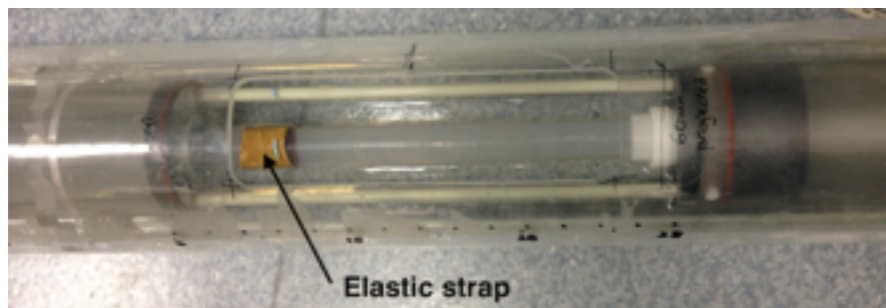
*Moireau, Xiao, Astorino, Figueroa, Chapelle, Taylor, JFG, (BMMB 2012)*  
*Moireau, Bertoglio, Xiao, Figueroa, Taylor, Chapelle, JFG, (BMMB 2013)*

# Application: arterial stiffness estimation

## Synthetic data



## Experimental data (KCL & Sheffield, euHeart)



## Clinical data

